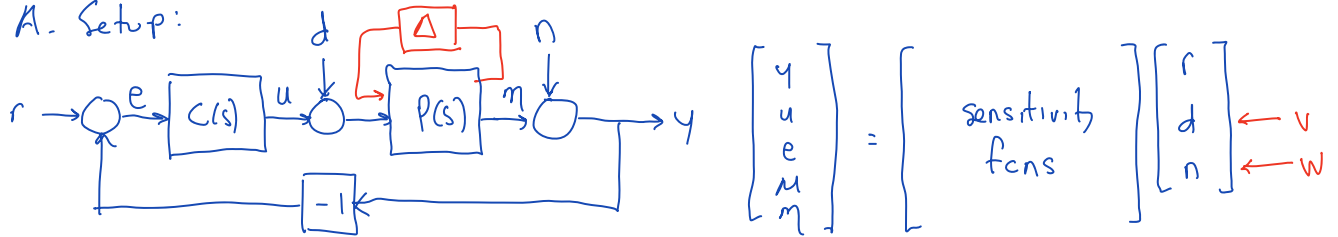


I. Sensitivity functions

A. Setup:



$$\begin{bmatrix} y \\ u \\ e \\ m \\ \eta \end{bmatrix} = \begin{bmatrix} \text{sensitivity} \\ \text{fncs} \end{bmatrix} \begin{bmatrix} r \\ d \\ n \end{bmatrix}$$

← v
← w

B. Alternative interpretation: process uncertainty Δ

$$G_{yd} = \frac{P}{1+PC} \quad \frac{dG_{yd}}{dP} = \frac{1}{1+PC} - \frac{PC}{(1+PC)^2} = \frac{1}{(1+PC)^2} = S \frac{G_{yd}}{P}$$

$$\Rightarrow \frac{dG_{yd}}{G_{yd}} = S \frac{dP}{P} \Rightarrow \text{relative change in } G_{yd} \text{ is given by "sensitivity"}$$

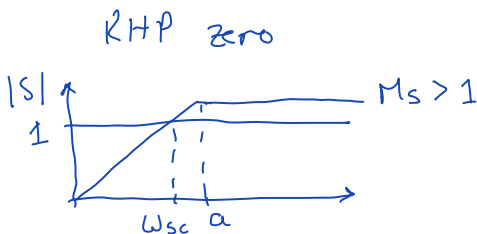
$$\text{Similarly } \frac{dG_{un}}{G_{un}} = -T \frac{dP}{P} \Rightarrow \text{relative change in } G_{un} \text{ given by "complementary sensitivity"}$$

$$S + T = 1 \Rightarrow \text{can't keep both small (at the same frequency)}$$

II. Limits of RHP poles and zeros

A. Maximum modulus thm: G analytic in Ω , $\sup_{s \in \Omega} |G(s)| = \sup_{\omega \in \mathbb{R}} |G(i\omega)|$

B. Application to RHP poles and zeros



$$S_r(s) = \frac{M_s s}{s+a}$$

Spec: $|S(i\omega)| \leq |S_r(i\omega)| \Rightarrow \left| \frac{S(i\omega)}{S_r(i\omega)} \right| \leq 1$

$$S(z) \frac{z+a}{M_s z} \leq \max_{\text{RHP}} \left| \frac{S(s)}{S_r(s)} \right| = \max_{\omega} \left| \frac{S(i\omega)}{S_r(i\omega)} \right| \leq 1$$

MMP spec

$$\Rightarrow a \leq z(M_s - 1) \quad \& \quad \omega_{sc} \leq z \sqrt{\frac{M_s - 1}{M_s + 1}} \leftarrow \text{via some algebra}$$

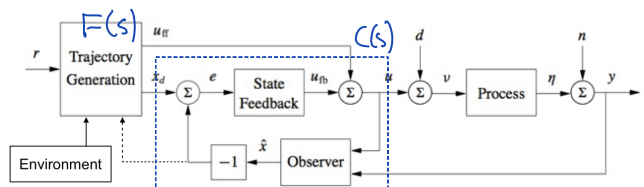
tradeoff!

- Implication: "slow" RHP zeros limit range over which S can be small
- Intuition via step response: have to wait for inverse response

- Similar result for RHP pole (acting on T)

- RHP pole & zero: can show $M_s \geq \left| \frac{z+p}{z-p} \right|$
 \Rightarrow nearby pole/zero very hard

- Important insight: zeros depend on sensor (C matrix)



III. Big picture (if time)