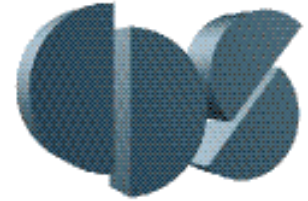




CDS 270-2: Lecture 3-1

Real-Time Trajectory Generation



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10 April 2006

Goals:

- Introduce two degree of freedom design for motion control systems
- Describe how to use flatness for real-time motion planning using NTG
- Give examples of implementation on Caltech ducted fan, satellite formations

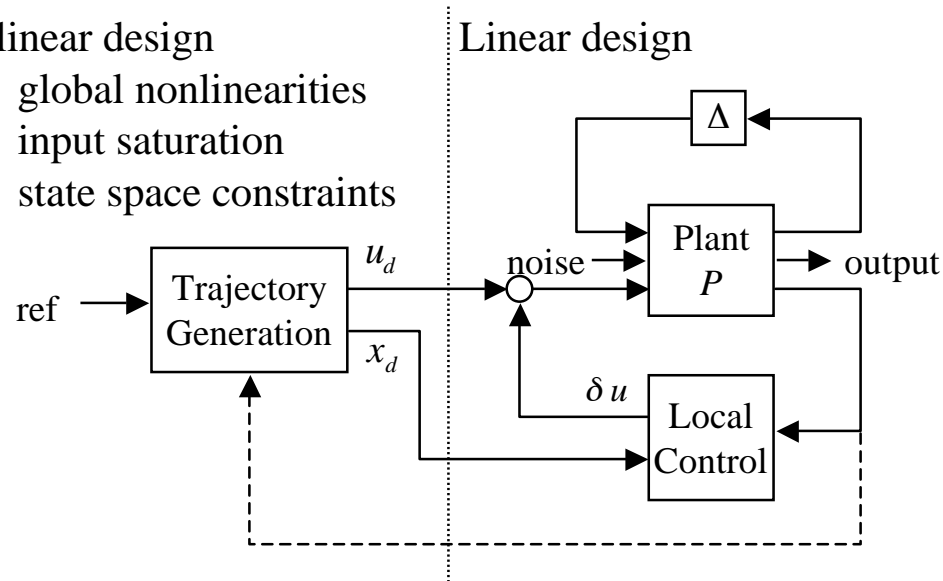
Reading:

- “A New Computational Approach to Real-Time Trajectory Generation for Constrained Mechanical Systems”, M. B. Milam, K. Mushambi and R. M. Murray. Conference on Decision and Control, 2000.
- “Inversion Based Constrained Trajectory Optimization”, N. Petit, M. B. Milam and R. M. Murray. IFAC Symposium on Nonlinear Control Systems Design (NOLCOS), 2001.

Real-Time Trajectory Generation Using Flatness

Nonlinear design

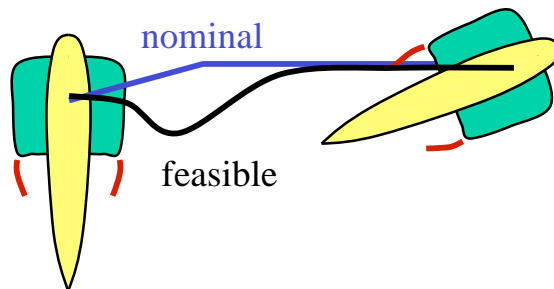
- global nonlinearities
- input saturation
- state space constraints



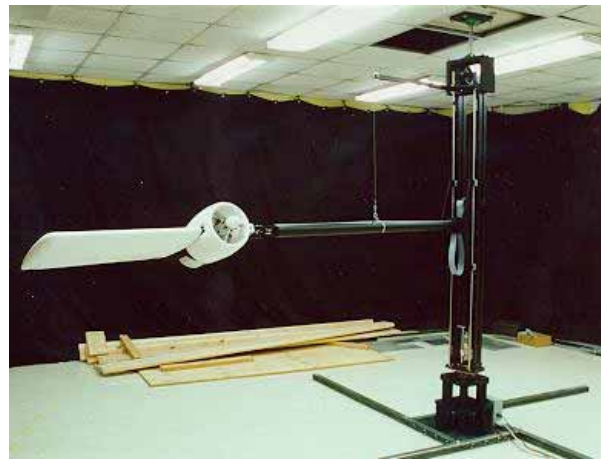
Approach: Two Degree of Freedom Design

- Use online trajectory generation to construct feasible trajectories
- Use linear control for local performance
- For many systems, dynamics are differentially flat \Rightarrow reduce dynamic system to algebraic equivalent and generate feasible trajectories in real time

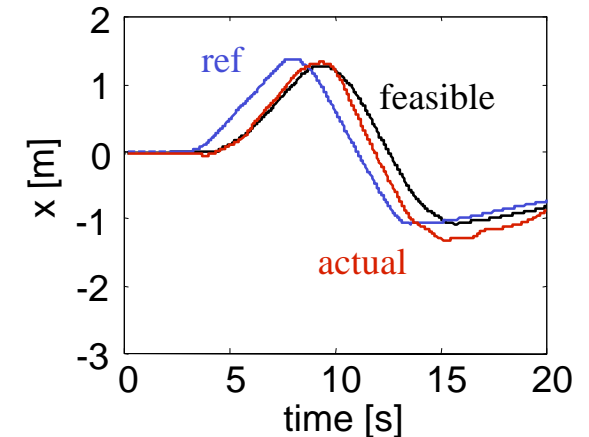
Rapid Transition from Hover to Forward Flight



Caltech Ducted Fan

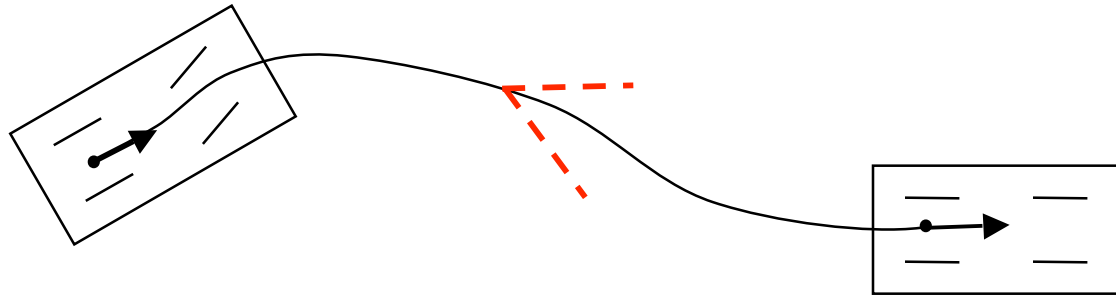


Real-Time Trajectory Generation



Trajectory Generation Using Differential Flatness

$$\begin{aligned}
 \mathfrak{z} &= f(x, u) & x &= x(z, \mathfrak{z}, \mathbf{K}, z^{(q)}) \\
 z &= h(x, u, \mathfrak{z}, \mathbf{K}, u^{(p)}) & u &= u(z, \mathfrak{z}, \mathbf{K}, z^{(q)}) \\
 |u| &< L & & \text{Complicated (algebraic) constraints}
 \end{aligned}$$



$$\bar{z}_0 = \begin{bmatrix} z(0) \\ \mathfrak{z}(0) \\ \mathfrak{z}^{(p)}(0) \\ \mathbb{M} \\ z^{(q)}(0) \end{bmatrix} \xrightarrow{z} \bar{z}_f = \begin{bmatrix} z(T) \\ \mathfrak{z}(T) \\ \mathfrak{z}^{(p)}(T) \\ \mathbb{M} \\ z^{(q)}(T) \end{bmatrix} \quad z = \sum \alpha_i \psi^i(t)$$

$$M\alpha = \begin{bmatrix} \bar{z}_0 \\ \bar{z}_f \end{bmatrix}$$

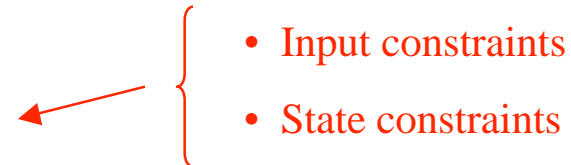
- Use basis functions to parameterize output \Rightarrow linear problem in terms of coefficients

Optimal Control Using Differential Flatness

Can also solve constrained optimization problem via flatness

$$\min J = \int_{t_0}^T L(x, u) dt + V(x(T), u(T))$$

subject to

$$\dot{x} = f(x, u) \quad g(x, u) \leq 0$$


- Input constraints
- State constraints

If system is flat, once again we get an *algebraic* problem:

$$\left. \begin{aligned} x &= x(z, \mathbb{K}, z^{(q)}) \\ u &= u(z, \mathbb{K}, z^{(q)}) \\ z &= \sum \alpha_i \psi^i(t) \end{aligned} \right\} \Rightarrow \left\{ \begin{aligned} \min J &= \int_{t_0}^T L(\alpha, t) dt + V(\alpha) \\ g(\alpha, t) &\leq 0 \\ &\text{Finite parameter optimization problem} \end{aligned} \right.$$

- Constraints hold at all times \Rightarrow potentially over-constrained optimization
- Numerically solve by discretizing time (collocation)

NTG: Nonlinear Trajectory Generation

Flatness-based optimal control package

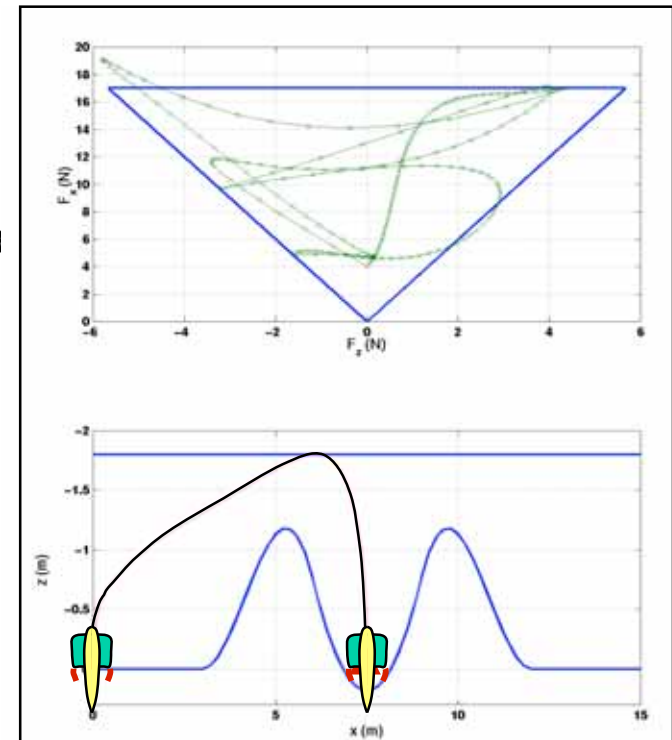
- B-spline representation of (partially) flat outputs
- Collocation based optimization approach
- Built on NPSOL optimization pkg (requires license)
- Warm start capability for receding horizon control

Solves general nonlinear optimization problem

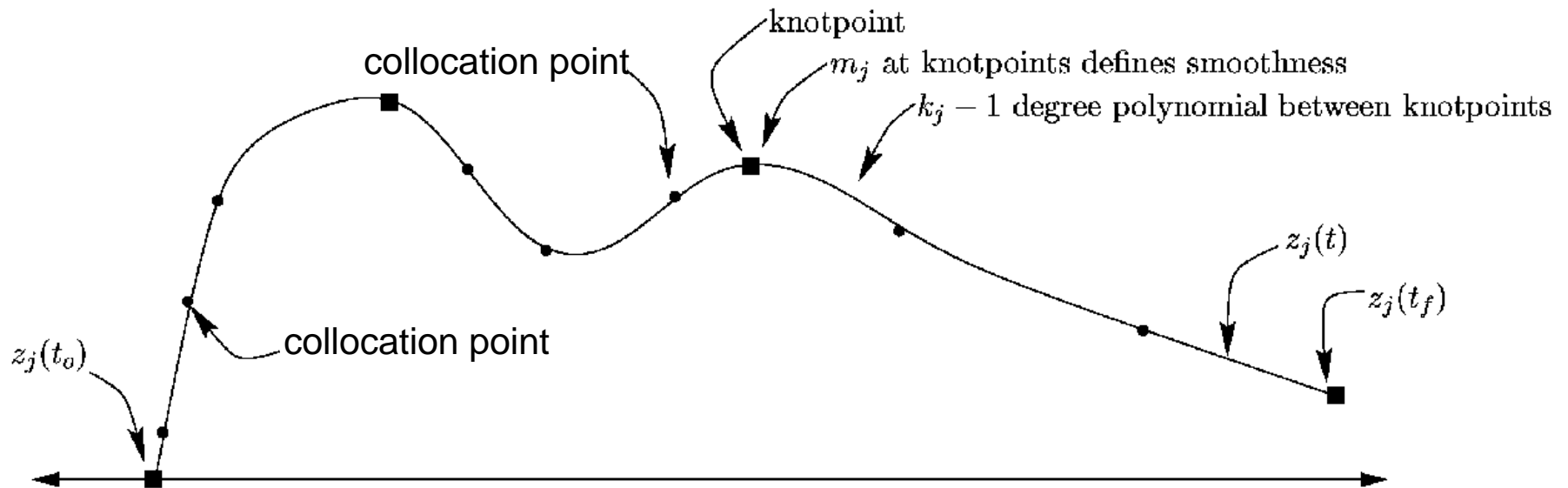
$$\min J = \int_{t_0}^T q(x, u) dt + V(x(T), u(T))$$
$$\dot{x} = f(x, u) \quad lb \leq g(x, u) \leq ub$$

- Assumes x and u are given in terms of (partially) flat outputs
- Constraints are enforced at a user-specified set of collocation points
- Gives *approximate* solution; need to use w/ feedback to ensure robustness (2 DOF)

http://www.cds.caltech.edu/~murray/software/2002a_ntg.html



Trajectory Generation Using Splines for Flat Outputs



Rewrite flat outputs in terms of splines

$$z_j = \sum_{i=1}^{p_j} B_{i,k_j}(t) C_i^j \quad \text{for the knot sequence } t_j$$

$$p_j = l_j(k_j - m_j) + m_j$$

Evaluate constrained optimization at collocation points:

$$\min_{\vec{C} \in \mathbb{R}^M} J(\bar{z}(t_i)) \quad \text{subject to} \quad lb \leq c(\bar{z}(t_i)) \leq ub$$

B_{i,k_j} = basis functions

C_i^j = coefficients

z_i = flat outputs

Application: Caltech Ducted Fan

Flight Dynamics

$$m\ddot{x} = -D \cos \gamma - L \sin \gamma + F_{X_b} \cos \theta + F_{Z_b} \sin \theta$$

$$m\ddot{z} = D \sin \gamma - L \cos \gamma - mg_{eff} + F_{X_b} \sin \theta + F_{Z_b} \cos \theta$$

$$J\ddot{\theta} = M_a - \frac{1}{r_s} I_p \Omega \dot{x} \cos \theta + M_T$$

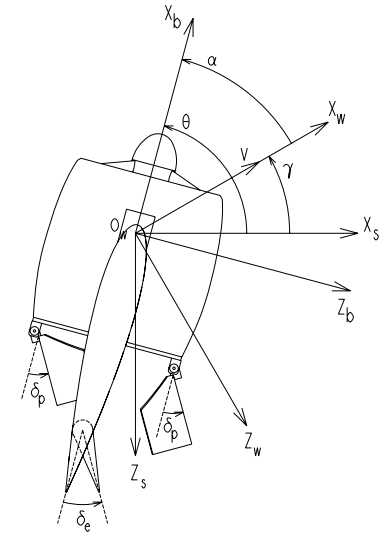
$$\alpha = \theta - \gamma, \quad \text{angle of attack}$$

$$\gamma = \tan^{-1} \frac{-\dot{z}}{\dot{x}}, \quad \text{flight path angle}$$

$$L = \frac{1}{2} \rho V^2 S C_L(\alpha)$$

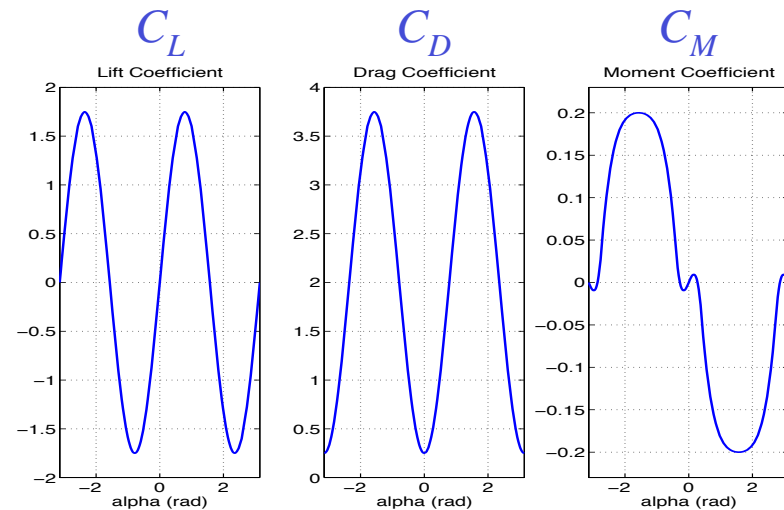
$$D = \frac{1}{2} \rho V^2 S C_D(\alpha)$$

$$M_a = \frac{1}{2} \bar{c} \rho V^2 S C_M(\alpha)$$



Trajectory Generation Implementation

- System is approximately flat, even with aerodynamic forces
- More efficient to over-parameterize the outputs; use $z = (x, y, \theta)$
- Input constraints: max thrust, flap limits, flap rates



Implementation using NTG Software Library

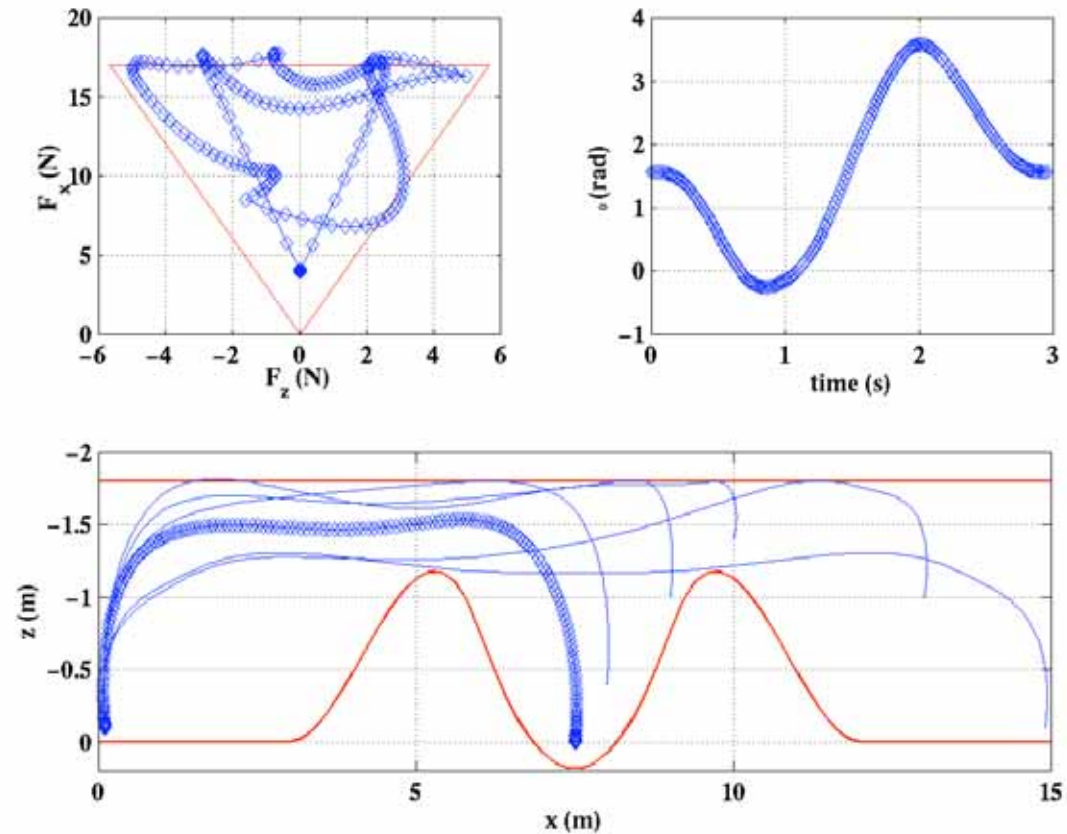
Features

- Handles constraints
- *Very fast* (real-time), especially from warm start
- Good convergence

Weaknesses

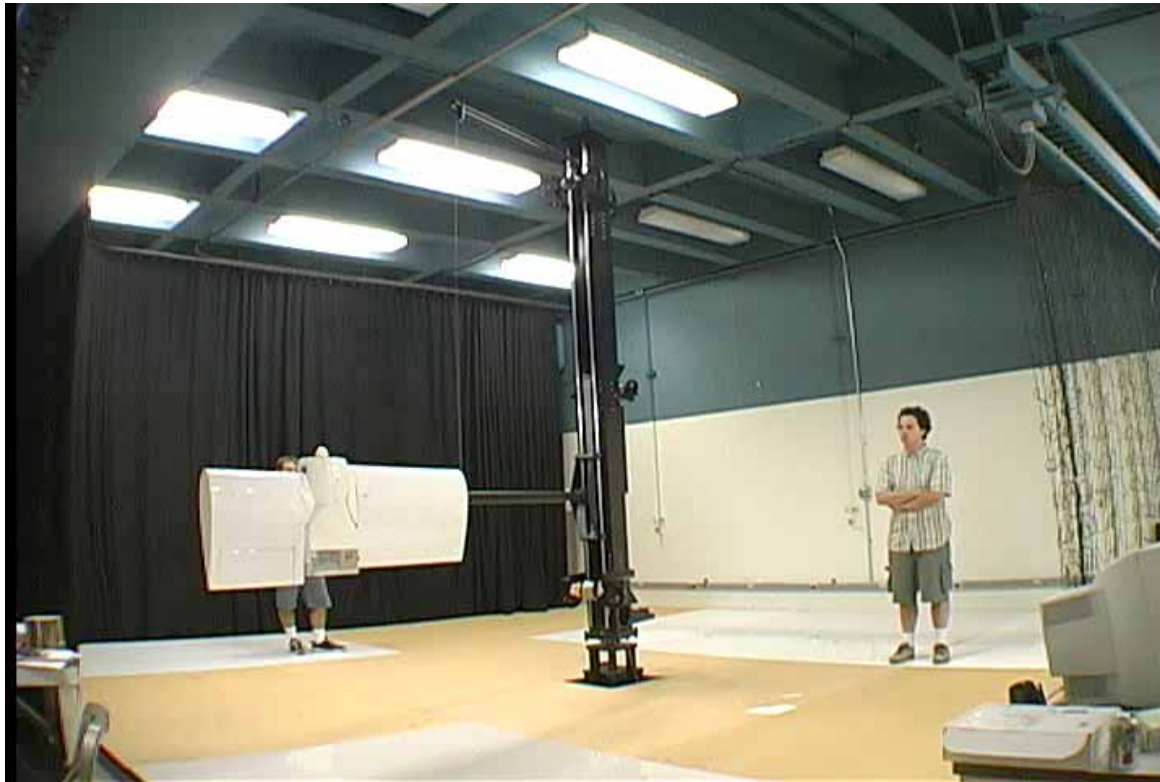
- No convergence proofs
- Misses constraints between collocation points
- Doesn't exploit mechanical structure (except through flatness)

Planar Ducted Fan: Warm Starts



http://www.cds.caltech.edu/~murray/software/2002a_ntg.html

Example 1: Trajectory Generation for the Ducted Fan



Caltech Ducted Fan

- Ducted fan engine with vectored thrust
- Airfoil to provide lift in forward flight mode
- Design to emulate longitudinal flight dynamics
- Control via dSPACE-based real-time controller

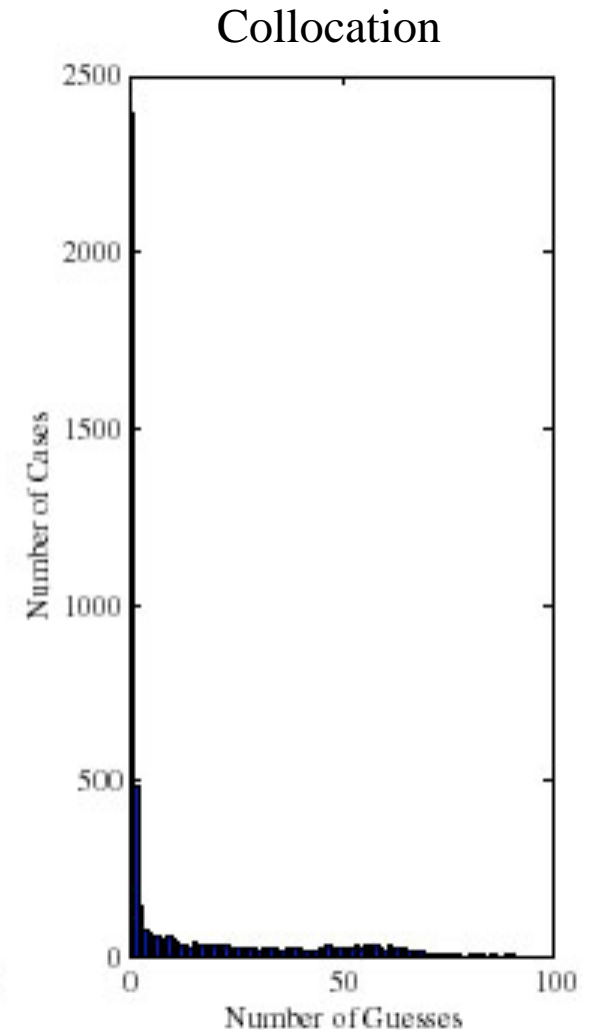
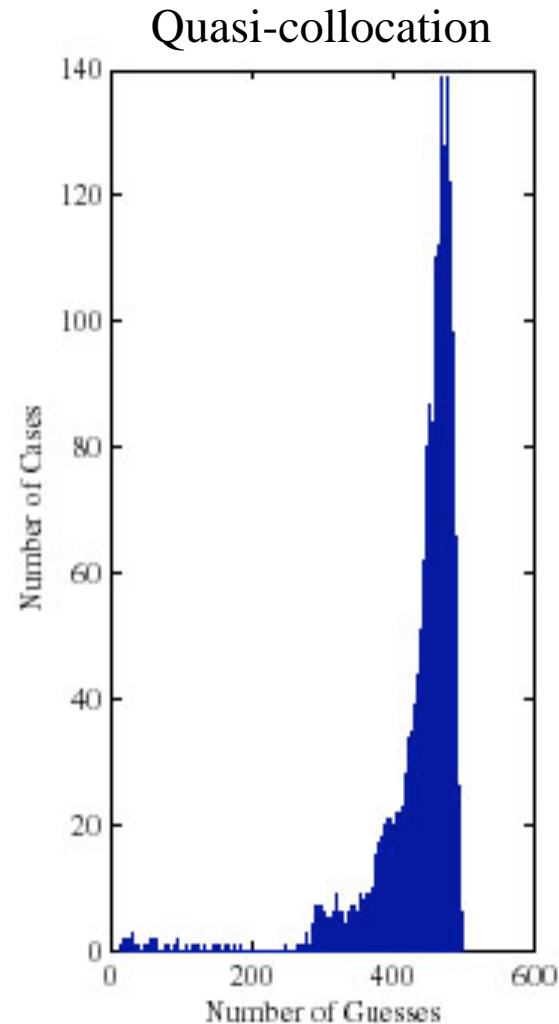
Trajectory Generation Task: point to point motion avoiding obstacles

- Use differential flatness to represent trajectories satisfying dynamics
- Use B-splines to parameterize trajectories
- Solve *constrained* optimization to avoid obstacles, satisfy thrust limits

NTG Convergence Properties

Numerical Studies using Caltech Ducted Fan

- 6461 test cases
- 500 initial guess for spline coefficients
- Total of > 3M runs
- Count # of cases that converge for given # of initial guesses
- Comparison between quasi-collocation (x , y , θ) and full collocation (states and inputs)



Trajectory Generation for Non-Flat Systems

If system is not fully flat, can *still* apply NTG

$$\begin{array}{l}
 \mathfrak{z} = f(x, u) \begin{cases} \longrightarrow z = z(x, u, \mathfrak{z}, \mathbb{K}, u^{(q)}) \\ \longrightarrow y = h(x, u) \end{cases} \longrightarrow \begin{array}{l} x = x(z, \mathfrak{z}, \mathbb{K}, z^{(q)}) \\ u = u(z, \mathfrak{z}, \mathbb{K}, z^{(q)}) \\ (x, u) = \Gamma(y, \mathfrak{z}, \mathbb{K}, y^{(q)}) \\ 0 = \Phi(y, \mathfrak{z}, \mathbb{K}, y^{(p)}) \end{array}
 \end{array}$$

When system is not flat, use *quasi-collocation*

- Choose output $y=h(x,u)$ that can be used to compute the full state and input
- Remaining dynamics are treated as *constraints* for trajectory generation
- Example: chain of integrators

$$\begin{array}{l}
 \mathfrak{z}_1 = x_2 \\ \mathfrak{z}_2 = u
 \end{array}
 \longrightarrow
 \begin{array}{l}
 y_1 = x_1 \\ y_2 = x_2
 \end{array}
 \longrightarrow
 \begin{array}{l}
 x_1 = y_1 \\ x_2 = y_2 \\ u = \mathfrak{z}_2
 \end{array}
 +
 \begin{array}{l}
 \mathfrak{z}_1 = y_2
 \end{array}
 \left. \vphantom{\begin{array}{l} \mathfrak{z}_1 = x_2 \\ \mathfrak{z}_2 = u \end{array}} \right\} \begin{array}{l} \text{Solve using} \\ \text{NTG with} \\ lb = ub \end{array}$$

Can also do full collocation (treat all dynamics as constraints)

$$\left. \begin{array}{l} (x, u) = \sum \alpha_i \psi^i(t) \\ \mathfrak{z}(t_i) = f(x(t_i), u(t_i)) \end{array} \right\} \begin{array}{l} \text{Each equation gives constraints at collocation} \\ \text{points} \Rightarrow \text{highly constrained optimization} \end{array}$$

Effect of Defect on Computation Time

Defect as a measure of flatness

- Defect = number of remaining differential equations
- Defect 0 \Rightarrow differentially flat

Sample problem: 5 states, 1 input

- x_1 is possible flat output
- Can choose other outputs to get systems with nonzero *defect*
- 200 runs per case, with random initial guess

Computation time related to defect through power law

- SQP scales cubically \Rightarrow minimize the number of free variables

Dramatic speedup through reduction of differential constraints

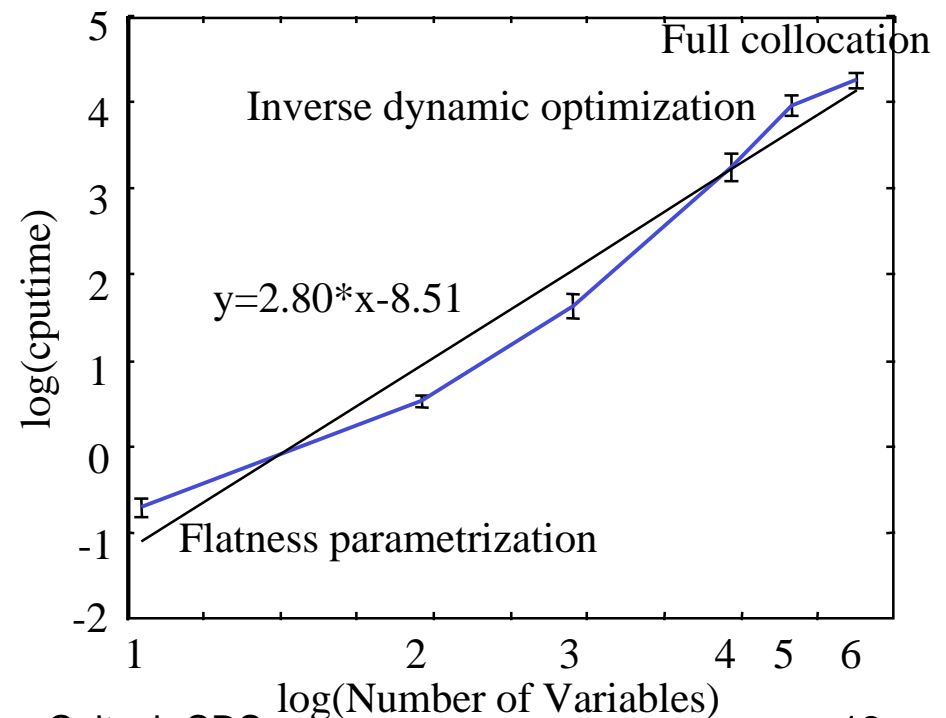
$$y_1 = 5x_2$$

$$y_2 = \sin x_1 + x_2^2 + 5x_3$$

$$y_3 = -x_1x_2 + x_3 + 5x_4$$

$$y_4 = x_1x_2x_3 + x_2x_3 + x_4 + 5x_5$$

$$y_5 = -x_5 + u$$

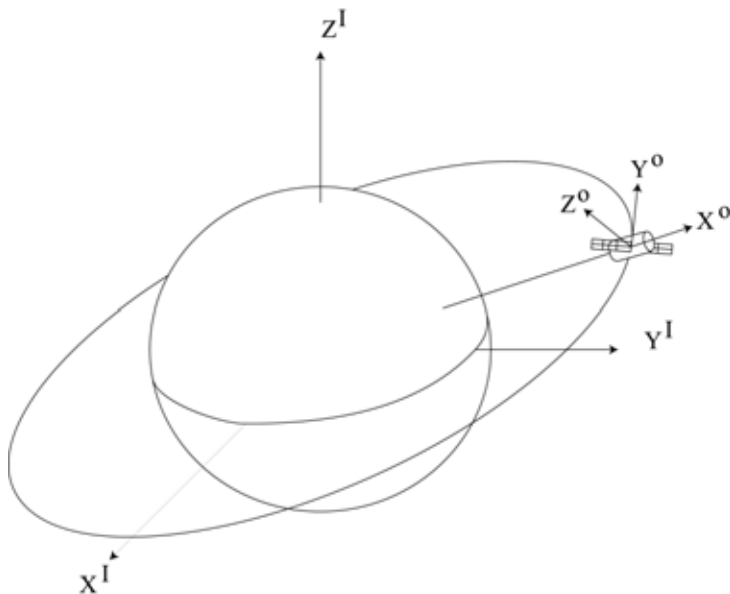


Example 2: Satellite Formation Control

Goal: reconfigure cluster of satellites using minimum fuel



Dynamics given by Hill's equations (fully actuated \Rightarrow flat)



$$\ddot{q}_1 = \frac{\mu q_1}{|\vec{q}|^3} - \frac{3J_2\mu R_e^2 q_1 (q_1^2 + q_2^2 - 4q_3^2)}{2|\vec{q}|^7} + u_1^I$$

$$\ddot{q}_2 = \frac{\mu q_2}{|\vec{q}|^3} - \frac{3J_2\mu R_e^2 q_2 (q_1^2 + q_2^2 - 4q_3^2)}{2|\vec{q}|^7} + u_2^I$$

$$\ddot{q}_3 = \frac{\mu q_3}{|\vec{q}|^3} - \frac{3J_2\mu R_e^2 q_3 (3q_1^2 + 3q_2^2 - 2q_3^2)}{2|\vec{q}|^7} + u_3^I$$

Satellite Formation Results

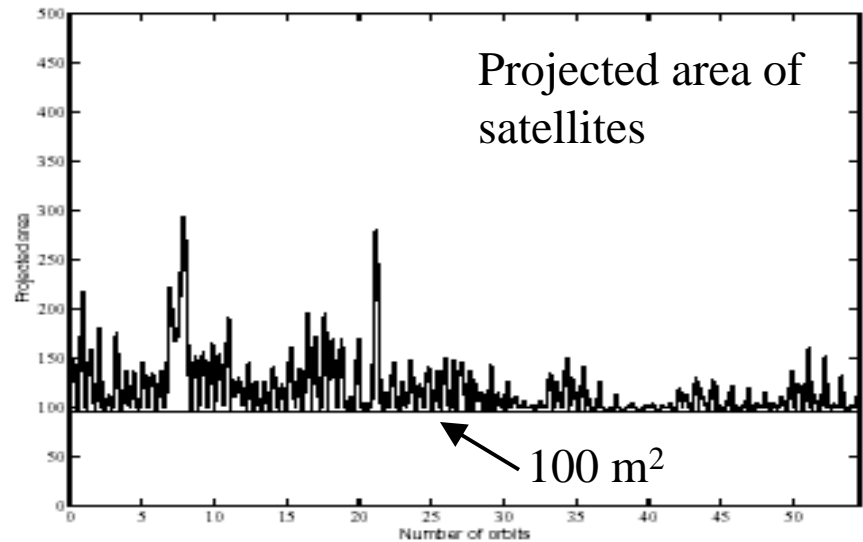
Station-keeping optimization

- Maintain a given area between the satellites (for good imaging) while minimizing the amount of fuel
- Idea: exploit natural dynamics of orbital equations as much as possible
- Input constraints: $\Delta V < 20$ m/s/year

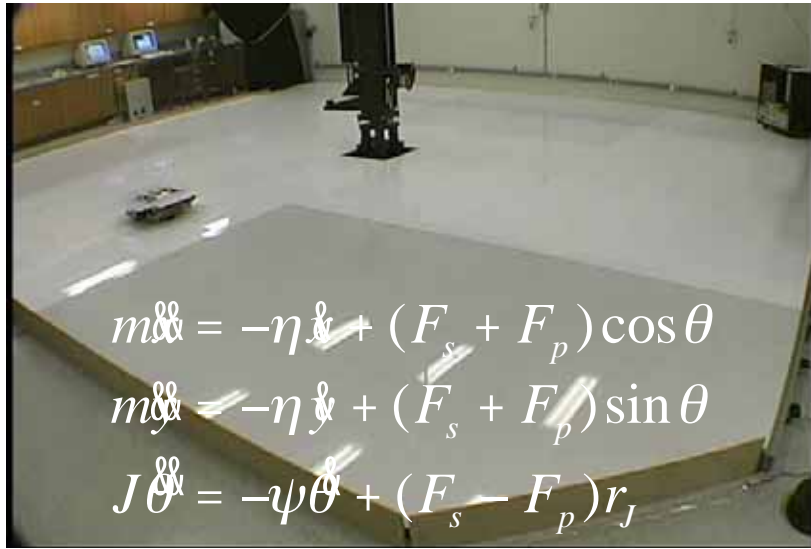
Results

- Use NTG to optimize over 60 orbits (~3 days), then repeat
- Results: at 45° inclination, obtain 10.4 m/s/year

$i = 0$ deg	$S = 100$ m ²	$S = 200$ m ²
$d \leq 500$ m	$\Delta V = 25.6$ m/s/year	$\Delta V = 47.8$ m/s/year
$i = 45$ deg	$S = 100$ m ²	$S = 200$ m ²
$d \leq 500$ m	$\Delta V = 10.4$ m/s/year	$\Delta V = 17.0$ m/s/year
$i = 90$ deg	$S = 100$ m ²	$S = 200$ m ²
$d \leq 500$ m	$\Delta V = 8.69$ m/s/year	$\Delta V = 21.4$ m/s/year



Example 3: MVWT Control Design

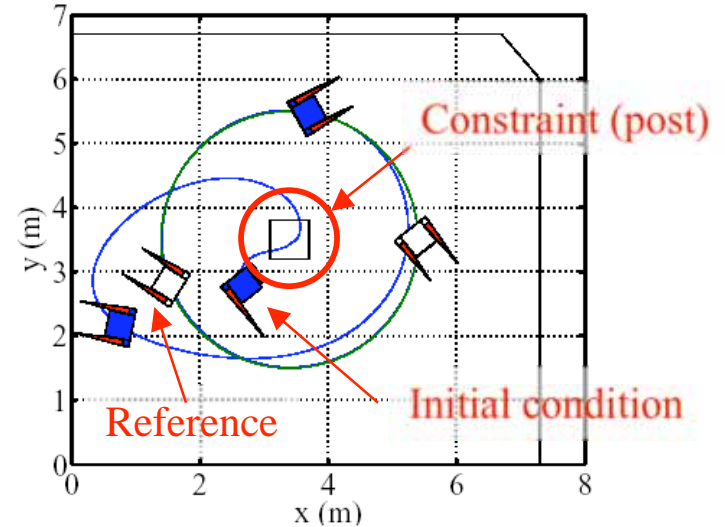


$$\begin{aligned} m\ddot{x} &= -\eta\dot{x} + (F_s + F_p)\cos\theta \\ m\ddot{y} &= -\eta\dot{y} + (F_s + F_p)\sin\theta \\ J\ddot{\theta} &= -\psi\dot{\theta} + (F_s - F_p)r_J \end{aligned}$$

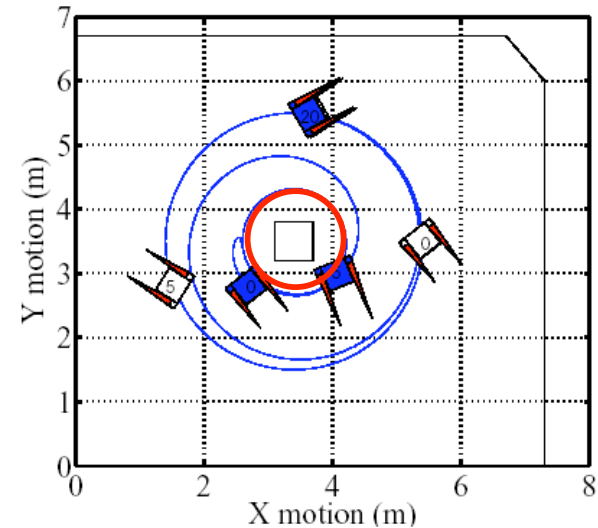
Control design technique

1. LQR design of state space controller K around reference velocity
 2. Choose P, Q, R using Kalman's formula
 3. Implement as a receding horizon control with input and state space constraints
- RHC controller respects state space constraint

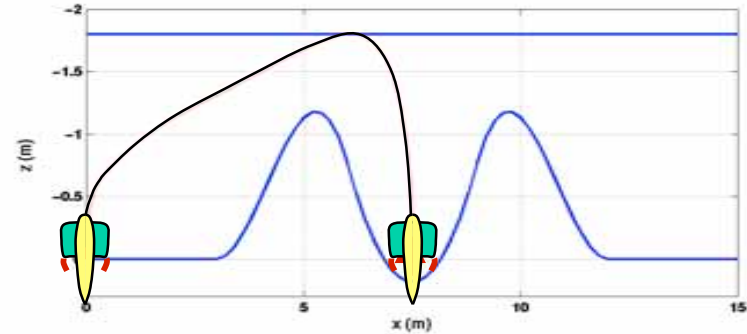
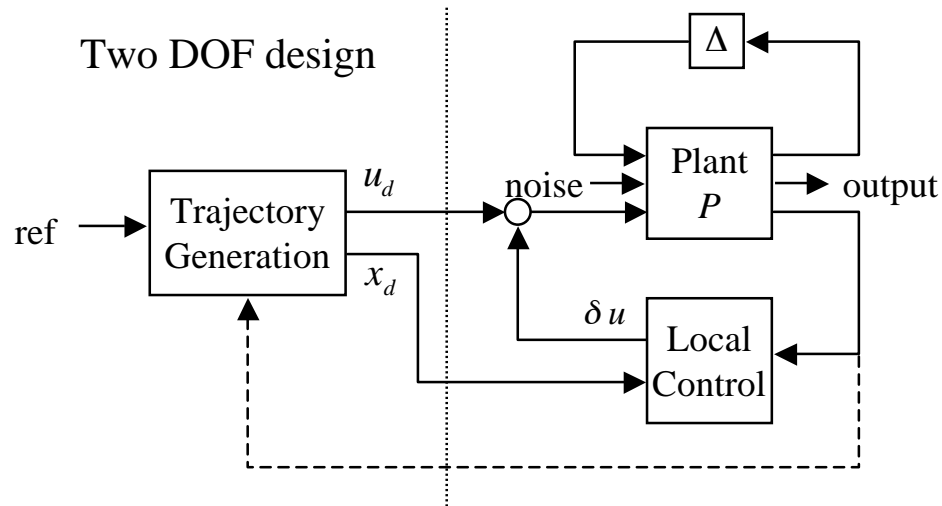
LQR control law



RHC control law



Summary: Real-Time Trajectory Generation



$$\min J = \int_{t_0}^T q(x, u) dt + V(x(T), u(T))$$

$$\dot{x} = f(x, u) \quad lb \leq g(x, u) \leq ub$$

Flatness is a key property for efficient motion planning

- Allows conversion of dynamics into algebra \Rightarrow much faster algorithms

NTG software package implements required calculations

- Allows solution of general constrained optimization, w/ parameterized outputs
- Gives *approximate* results \Rightarrow need to use in feedback context (not open loop)

Growing collection of applications

- Caltech ducted fan, satellite formation control
- Underwater vehicles, wheeled mobile robots, RoboFlag, Alice, ...

Homework and Project Ideas

Homework

- Download NTG and implement the point to point motion control problem for Alice or a RoboFlag vehicle.

Project ideas:

- For multi-vehicle applications, need to distribute the computation across multiple computers
- Use spread to implement a distributed trajectory generation capability

