Dynamical Systems, Optimal Control, and Microsat Formation Flight

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Control and Dynamical Systems

Five Objectives of Microsat

- \Box 1. Dynamics of multiple spacecraft in nearby orbits
- \Box 2. Formation stabilization strategies
- \Box 3. Formation reconfiguration algorithms
- \Box 4. Mathematical modeling and simulation tools
- \Box 5. Power requirements and limitations

Information

URL's

- □ http://www.cds.caltech.edu/microsat/
- □ http://www.cds.caltech.edu/~marsden/
- http://www.cds.caltech.edu/~murray/

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Team

 Faculty: Jerry Marsden, Richard Murray, CIT, Meir Pachter, Air Force Institute of Technology
 Postdocs: Wang-Sang Koon, David Chichka,
 Graduate Students: Dong-Eui Chang, Alex Fax, Mark Milam, Bill Dunbar, plus other student help

Related Activities with JPL

Genesis Discovery Mission

□ Uses 3-body problem libration point dynamics and heteroclinic connections

Jovian moon missions

□ Uses transfers between different 3-body problem libration point dynamics

Terrestrial Planet Finder

 \Box Uses coordinated control and 3-body dynamics

Development of LTool

 \Box software for libration point missions

Posters

Nonlinear Dynamics & Formation Flight

- □ Study of candidate reference orbits whose nearby orbits may support formation flight
- \Box Development of a geometric mechanics framework for the Kepler- J_2 dynamics

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Nonlinear Dynamics & Formation Flight

- □ Study of candidate reference orbits whose nearby orbits may support formation flight
- \Box Development of a geometric mechanics framework for the Kepler- J_2 dynamics
- Control and Optimal Control of Formation Flight
 - Optimal control for formation reconfiguration
 - \Box Cooperative control
 - \Box Lyapunov-based global orbit transfer

Three Topics

\Box Dynamics of satellites in Earth orbit

- \Box Cluster reconfiguration
- \Box Orbital transfer.

A Few Key References

- Broucke, R. A. [1994] Numerical integration of periodic orbits in the main problem of artificial satellite theory. Celestial Mech. Dynam. Astronom. 58 (1994), 99–123.
- Chobotov, V.A. [1991] Orbital Mechanics, AIAA.
- Coffey, D., A. Deprit, and B. Miller [1986] The critical inclination in artificial satellite theory, Celest. Mech., 39, 365–405.
- Cushman, R.H. [1991] A survey of normalization techniques applied to perturbed Keplerian systems, Dynamics Reported, 1, 54–112.
- Golubitsky, M., I. Stewart, and J. Marsden [1987] Generic bifurcation of Hamiltonian systems with symmetry, Physica 24D, 391–405.
- Marsden, J. E., R. Montgomery and T. S. Ratiu [1990] Reduction, symmetry and phases in mechanics, Memoirs of the AMS, 436.
- Marsden, J.E. and T.S. Ratiu [1999] Introduction to Mechanics and Symmetry. Texts in Applied Math., 17, Springer-Verlag, 1994. Second Ed., 1999.
- Moser, J. [1970] Regularization of Kepler's problem and the averaging method on a manifold, Commun. on Pure and Applied Math., 23, 609–636.
- Prussing, J.E. and B.A. Conway [1993] Orbital mechanics. Oxford Univ. Press.
- Vinti, J.P. [1998] Orbital and celestial mechanics, AIAA.

Basic J_2 dynamics

Satellite in Earth orbit

□ motion in Kepler potential plus J_2 perturbation □ $J_2 = bulge of the Earth$

I_2 causes

- \Box a drift in the orbit plane (geometric phase)
- \Box a drift in the major axis of the ellipse within the (approximate) orbital plane (direction of drift depends on the angle of inclination)

Basic J_2 dynamics



Basic J_2 dynamics



ORBIT SWINGS WESTWARD

Example: inclination = 28 degrees, altitude 300km period of Ω = roughly 50 days (left) period of ω = roughly 30 days (right).

Poincaré Sections

- Shows rich nonlinear dynamics
- **Relative to rotations around the** *z***-axis**
 - □ Involves Routh reduction; one studies orbits for various energies h and angular momenta ν about the z-axis.
 - \Box Original problem 6 dimensional: constant h and ν and remove angular variable gives 3 and a Poincaré section in that is 2-dimensional.

Poincaré Sections



Poincaré maps for the J_2 problem (Broucke, 1992)

Relative Motions

- □ Poincaré sections useful for detecting bifurcations.
- \Box What about relative motions?
 - Are there relative motions that remain tied together?
 - Not obvious because of phase drifts, etc.
- \Box To answer this we need to have a closer look at the dynamics and the role of reduction theory.
- □ Indeed, there are such interesting orbits (see the posters for details)

Relative Motions



Relative dynamics (100 days) of a satellite in a frame moving with a reference satellite

Geometric Mechanics and J_2

Reduction theory

- \Box all the crucial features (Ω -drift as a geometric phase etc) come out naturally
- \Box gives a global picture of the dynamics.

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Symmetries

rotational S¹ symmetry about the vertical axis.
 A Z₂ symmetry—reflection in the equatorial plane
 Another Z₂ symmetry—reflection in vertical planes
 + time reversal—an antisymplectic symmetry.

Moser Regularization

- \Box Kepler Hamiltonian H_0 and dynamics transferred to geodesics on S^3 .
- \Box Symmetry group is now SO(4)
- □ Momentum map includes the Laplace-Runge-Lenz vector (a vector pointing to the periapsis):

$$(\mathbf{r}, \dot{\mathbf{r}}) \mapsto (\mathbf{L}, \mathbf{A}) = \left(\mathbf{r} \times \dot{\mathbf{r}}, \ \dot{\mathbf{r}} \times (\mathbf{r} \times \dot{\mathbf{r}}) - \mu \frac{\mathbf{r}}{\|\mathbf{r}\|}\right)$$

Symmetry & Reduction

 \Box On an energy surface, Keplerian orbits are closed with the same period—Kepler flow gives an S^1 action

 \Box Total Hamiltonian is a sum:

$$H = H_0 + \epsilon H_1; \quad \epsilon = J_2$$
 size

- \Box Average with respect to the Keplerian S^1 action.
- □ Averaged Hamiltonian has symmetry

 $S^1 \times S^1 \times \mathbb{Z}_2 \times \mathbb{Z}_2.$

- $\Box \ Double$ reduction–a Keplerian S^1 symmetry and an axial S^1 symmetry
- Discrete symmetries pass to the reduced space

Symmetry & Reduction



Final Reduced Space– S^2

- flow parametrized by (Keplerian) energy h and ν
 bifurcations as h and ν are varied; bifurcation occurs at the critical inclination: h² 5ν² = 0
 fixed points on S² = periodic orbits on S³
 singularity if angular momentum ν = 0; singular points are orbits that head directly into poles
- \Box can use *energy-momentum* methods for stability and bifurcation
- \Box figures show a series of reduced phase portraits for fixed h as ν decreases to zero.

Final Reduced Space– S^2



h/√5 < ν < h
 0 < ν < h/√5, (bifurcation at critical inclination)
 ν near zero, 4. ν = 0 (singular case).

Variational integrators

- variational (symplectic) algorithms are remarkably good in many problems, especially for long term, sensitive integrations
- □ need to use symmetry properly
- \Box We have developed a reduction theory for discrete mechanics and have applied the associated variational integrators to the J_2 problem.

Loose control

□ For example, the simultaneous in situ measurement of the magneto-sphere may require a loose constellation scattered all over the magneto-sphere.

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Precision control

□ For interferometry, the shape and orientation of the formation must be maintained to some degree.

 \Box Either

- one has to maintain it very precisely or
- one has to **know** the relative positions precisely so that this information can be managed in software.

Performance Metrics

• 1. *Coverage analysis*—estimate of the amount of data collected. Based on this metric, one could then make quantitative tradeoff studies and compare different designs.



- 2. **Propulsion requirements**—the use of natural dynamics greatly affects this.
- 3. *Power requirements*-eg, battery size contributes significantly to the mass of the spacecraft.
- 4. **Spacecraft mass**-depends not only on the trajectory design, control algorithm, propulsion and power subsystems, but also on the launch vehicle capability and launch deployment strategy.

Formation Maintenance

- □ Natural dynamics plays a critical role.
- □ since only small changes are presumably needed, standard *linear control techniques* should be adequate for maintenance.
- □ one still needs to deal with cooperative techniques as well as possible combinatorial explosions. Graph theoretic methods probably useful.
- Utilize the fact that this is a problem with two greatly differing scales: the relative distances between the satellites (the *shape dynamics*) and the absolute position of the cluster as a whole. Geometric mechanics can help in the separation of these effects.

Formation Reconfiguration

More challenging

- \Box Larger dynamic motions are involved
- **Example:** reorient the whole formation
- \Box Fuel useage is potentially critical

Optimal control

- \Box Requires a good first guess
- \Box Works best when used with the natural dynamics

Two examples

 Trajectory correction maneuvers (TCM) for halo orbit insertion
 Earthbound satellite reconfiguration

TCM for Halo Orbit Insertion

- □ Optimization software used is COOPT: (COntrol–OPTimization)
- □ Optimizes: cost function = ΔV subject to the constraint of the equations of motion.
- □ We vary the number of impulses and also consider the effect of *delaying the first impulse and the launch uncertainty*.
- □ Makes use of the dynamical systems structure of the three body problem (especially the invariant manifolds of halo orbits).

Movie-Optimal Insertion

movie insert

Sensitivity Analysis



Varying launch velocity and first manouver delay

Alternative software for the reconfiguration problem

- \Box **NTG** (nonlinear trajectory generation)
- \Box Also uses direct (brute force) optimization
- □ key difference with COOPT: substitutes the forces using the equations of motion, so one gets a *higher order cost function*
- avoids treating the equations of motion as constraints (horrors!)

Sample problem

- Consider the toy problem of the equations linearized about a circular orbit *without any* J_2 *effect*.
- □ This is *not realistic*, but it is a demonstration that *the software is effective*.
- □ More generally, one would have to use the full nonlinear equations about a nominal trajectory family.
- □ Linearization methods here may not be adequate, but the sofware treats the nonlinear problem with no difficulty.

- □ Specific Objective: Find a trajectory that minimizes the control energy, over a fixed time, for three microsats such that at the final configuration the the microsats will remain on a circle (projection onto the yz plane) of 100 m radius, 120 degrees apart with no control force, indefinitely.
- Use a *rotating frame* with coordinate axes so that the x-axis is along the line of sight from the earth, while the y-axis is along the orbit and z is perpendicular to these two. The yz plane is what you see looking up from the Earth.

Cost Function: minimize

$$J = \int_0^T \sum_{i=1}^3 \left(|a_{x_i}|^2 + |a_{y_i}|^2 + |a_{z_i}|^2 \right) dt$$

Equations of Motion in normalized coordinates:

$$\begin{aligned} \ddot{x}_i &= 2\dot{y}_i + 3x_i + a_{x_i} \\ \ddot{y}_i &= -2\dot{x}_i + a_{y_i} \\ \ddot{z}_i &= z + a_{z_i}, \end{aligned}$$

where (x_i, y_i, z_i) is the position of the *i*th satellite, i = 1, ... 3 relative to the reference circular orbit.

□ Note that if one substitutes from the equations of motion, then one gets a cost function that depends on second order derivatives.

□ Final Time Constraints: Satellites should move in the known circular solutions of the equations that lie in the plane 2x + z = 0 with line of sight radius chosen to be R = 100m.

Optimal Reconfiguration

3D movie insert

Optimal Reconfiguration

Earth movie insert

Information Exchange

- □ The optimal reconfigurations above assume, implicitly, a centralized controller with full state information.
- □ Can formations (nearly) recover optimal trajectories through minimum transfer of information between satellties (or vehicles) when only certain avenues of communication and sensing are available?
- □ The communication topology and information flow design are important questions.

Example: six cars asked to acquire points on a regular hexagon (relative to one another) where each car can only sense its position relative to another car and can only communicate with one other car.

Information Exchange

• Movie 1 shows the solution for the hexagon problem when the only sensing information available to each car is the relative position of the car behind.

Information Exchange

• Movie 2 shows the solution when, in addition, some message passing from cars to cars ahead of them is available. (Reasonably close to the optimal solution).

Key Features

- □ Method of orbit transfer for the Kepler problem with thrust control, based on Lyapunov stability theory.
- \Box Makes use of the conserved quantities of the Kepler motion; the angular momentum **L** and the Laplace-Runge-Lenz vector **A**.
- □ Traditionally, orbit transfer is designed using conicsection geometry and orbital elements. No guarantee of convergence.
- □ The controller we design makes it possible to use continuous thrust so that we can do orbit transfer without necessarily using a large impulsive thrust.

- Lyapunov-based methods are efficient, guarantees convergence and reduces to many well known cases such as transfer between circular orbits and a onepulse inclination change.
- \Box Basic: ${\bf L}$ and ${\bf A}$ uniquely specify a Keplerian orbit.

Some key points

 \Box Equation of the motion with control

$$\ddot{\mathbf{r}} = -\mu \frac{\mathbf{r}}{\|\mathbf{r}\|^3} + \mathbf{F}$$

where \mathbf{F} is the control force.

 \Box Fix a Kepler orbit with a given target value ($\mathbf{L}_T, \mathbf{A}_T$).

 \Box Define $V : \mathbb{R}^3 \times \mathbb{R}^3 \to \mathbb{R}$ by $V(\mathbf{L}, \mathbf{A}) = \frac{1}{2} a \left\| \Delta \mathbf{L} \right\|^2 + \frac{1}{2} \left\| \Delta \mathbf{A} \right\|^2,$ where $\Delta \mathbf{L} = \mathbf{L} - \mathbf{L}_T$, $\Delta \mathbf{A} = \mathbf{A} - \mathbf{A}_T$ and a > 0. \Box Use the equations of motion and $\dot{\mathbf{L}} = \mathbf{r} \times \mathbf{F}, \qquad \mathbf{A} = \mathbf{F} \times \mathbf{L} + \dot{\mathbf{r}} \times (\mathbf{r} \times \mathbf{F}).$ to compute the time derivative of VDesign the controller accordingly: $\mathbf{F}(\mathbf{r}, \dot{\mathbf{r}}, t; \mathbf{L}_T, \mathbf{A}_T) =$ $-f(\mathbf{r}, \dot{\mathbf{r}}, t) \left(a \Delta \mathbf{L} \times \mathbf{r} + \mathbf{L} \times \Delta \mathbf{A} + (\Delta \mathbf{A} \times \dot{\mathbf{r}}) \times \mathbf{r} \right)$ with $f(\mathbf{r}, \dot{\mathbf{r}}, t) > 0$ suitably chosen.

Planar transfer between two coplanar circular orbits of radii 1 and 2.

Orbit Transfer Movie

The End

The End

TYPESETTING SOFTWARE: TEX, Textures, LATEX, hyperref, texpower, Adobe Acrobat 4.05 ILLUSTRATIONS & MOVIES: Adobe Illustrator 8.0, Mathematica, MATLAB, QuickTime, and other tools LATEX SLIDE MACRO PACKAGES: Wendy McKay, Ross Moore