



CDS 110b: Lecture 2-1

Linear Quadratic Regulators



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Goals:

- Derive the linear quadratic regulator and demonstrate its use

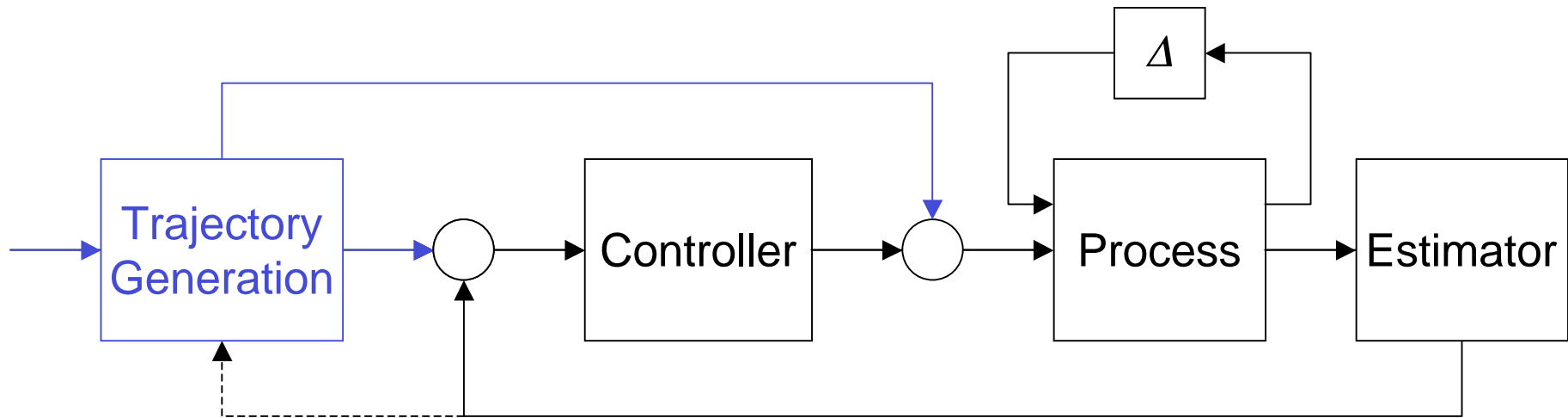
Reading:

- Friedland, Chapter 9 (different derivation, but same result)
- RMM course notes (available on web page)
- Lewis and Syrmos, Section 3.3

Homework #2

- Design LQR controllers for some representative systems
- Due Wed, 18 Jan by 5 pm, in box outside 109 Steele

Review from last lecture



Trajectory Generation via Optimal Control:

$$\begin{aligned} \dot{x} &= f(x, u) \quad x \in \mathbb{R}^n \\ x(0) &\text{ given} \quad u \in \Omega \subset \mathbb{R}^p \end{aligned}$$

$$\begin{aligned} J &= \int_0^T L(x, u) dt + V(x(T)) \\ \psi(x(T)) &= 0 \end{aligned}$$

Today: focus on special case of a linear quadratic regulator

$$\begin{aligned} \dot{x} &= Ax + Bu \quad x \in \mathbb{R}^n \\ x(0) &\text{ given} \quad u \in \mathbb{R}^p \end{aligned}$$

$$\begin{aligned} J &= \int_0^T x^T Q x + u^T R u dt + x(T)^T P_1 x(T) \\ &\text{no terminal constraints} \end{aligned}$$

Linear Quadratic Regulator (finite time)

Problem Statement

$$\begin{aligned} \dot{x} &= Ax + Bu & x &= \mathbb{R}^n \\ x(0) &\text{ given} & u &\in \mathbb{R}^p \end{aligned} \quad \tilde{J} = \frac{1}{2} \int_0^T (x^T Q x + u^T R u) dt + \frac{1}{2} x^T(T) P_1 x(T)$$

- Factor of 1/2 simplifies some math below; optimality is not affected

Solution: use the maximum principle

$$H = x^T Q x + u^T R u + \lambda^T (Ax + Bu)$$

$$\begin{aligned} \dot{x} &= \left(\frac{\partial H}{\partial \lambda} \right)^T = Ax + Bu & x(0) &= x_0 \\ -\dot{\lambda} &= \left(\frac{\partial H}{\partial x} \right)^T = Qx + A^T \lambda & \lambda(T) &= P_1 x(T) \\ 0 &= \frac{\partial H}{\partial u} = Ru + \lambda^T B & \implies & u = -R^{-1} B^T \lambda. \end{aligned}$$

- This is still a two point boundary value problem \implies hard to solve
- Note that solution is linear in x (because λ is linear in x , treated as an input)

Simplified Form of the Solution

Can simplify solution by guessing that $\lambda = P(t) x(t)$

$$-\dot{\lambda} = \left(\frac{\partial H}{\partial x} \right)^T = Qx + A^T \lambda \quad \lambda(T) = P_1 x(T) \quad \leftarrow \text{From maximum principle}$$

$$\dot{\lambda} = \dot{P}x + P\dot{x} = \dot{P}x + P(Ax - BR^{-1}B^T P)x \quad \leftarrow \text{Substitute } \lambda = P(t) x(t)$$

↓

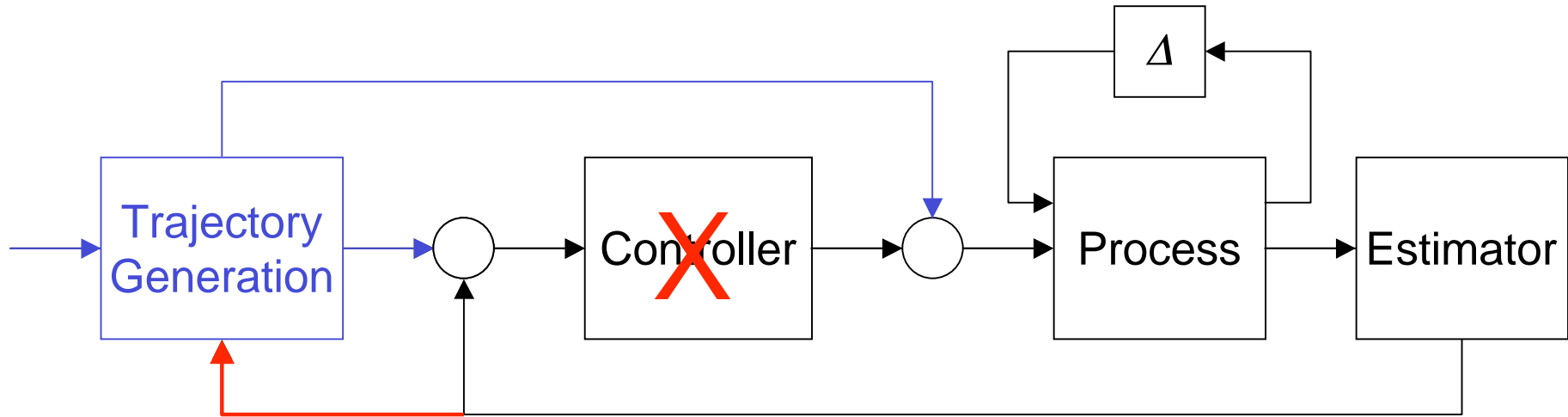
$$-\dot{P}x - PAx + PBR^{-1}BPx = Qx + A^T Px.$$

Solution exists if we can find $P(t)$ satisfying

$$-\dot{P} = PA + A^T P - PBR^{-1}B^T P + Q \quad P(T) = P_1$$

- This equation is called the *Riccati ODE*; matrix differential equation
- Can solve for $P(t)$ backwards in time and then apply $u(t) = -R^{-1} B^T P(t) x$
- Solving $x(t)$ forward in time gives optimal state (and input): $x^*(t), u^*(t)$
- Note that $P(t)$ can be computed once (ahead of time) \Rightarrow allows us to find the optimal trajectory from different points just by re-integrating state equation with optimal input

Finite Time LQR Summary



Problem: find trajectory that minimizes

$$\begin{aligned} \dot{x} &= Ax + Bu & x &\in \mathbb{R}^n \\ x(0) &\text{ given} & u &\in \mathbb{R}^p \end{aligned} \quad \tilde{J} = \frac{1}{2} \int_0^T (x^T Q x + u^T R u) dt + \frac{1}{2} x^T(T) P_1 x(T)$$

Solution: time-varying linear feedback

$$u(t) = -R^{-1} B P(t) x.$$

$$-\dot{P} = PA + A^T P - P B R^{-1} B^T P + Q \quad P(T) = P_1$$

- **Note: this is in feedback form \Rightarrow can actually eliminate the controller (!)**

Infinite Time LQR

Extend horizon to $T = \infty$ and eliminate terminal constraint:

$$\begin{aligned} \dot{x} &= Ax + Bu & x &= \mathbb{R}^n \\ x(0) &\text{ given} & u &\in \mathbb{R}^p \end{aligned} \quad J = \int_0^\infty (x^T Q x + u^T R u) dt$$

Solution: same form, but can show P is constant

$$\begin{aligned} u &= Kx & K &= -R^{-1}B^T P && \longleftarrow \text{State feedback (constant gain)} \\ 0 &= PA + A^T P - PBR^{-1}B^T P + Q && && \longleftarrow \text{Algebraic Riccati equation} \end{aligned}$$

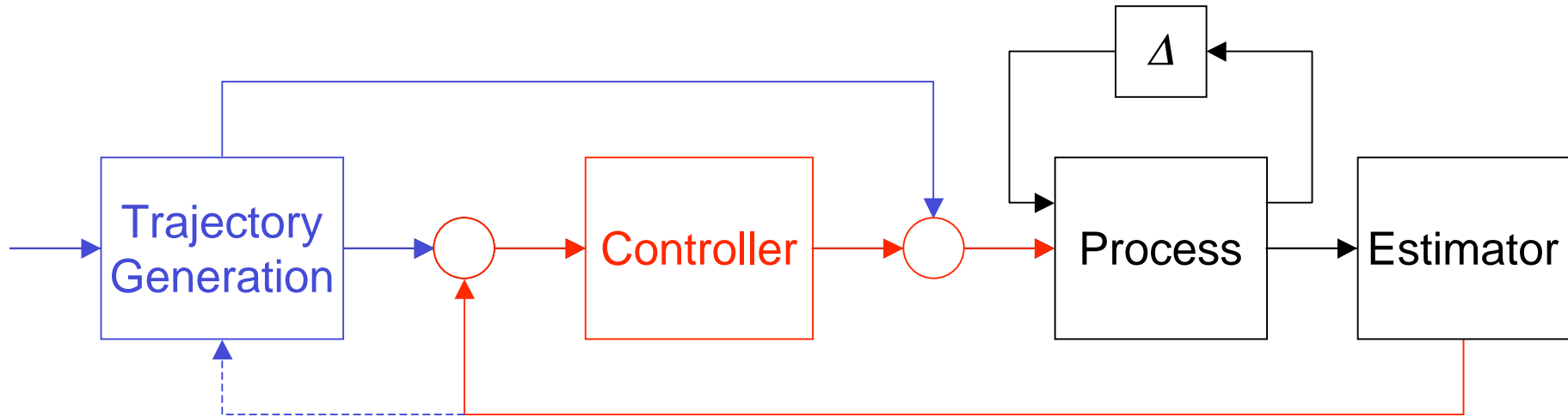
Remarks

- In MATLAB, $K = \text{lqr}(A, B, Q, R)$
- Require $R > 0$ but $Q \geq 0$ + must satisfy “observability” condition
- Alternative form: minimize “output” $y = Hx$

$$L = \int_0^\infty x^T H^T H x + u^T R u dt = \int_0^\infty \|Hx\|^2 + u^T R u dt$$

- Require that (A, H) is observable. Intuition: if not, dynamics may not affect cost \Rightarrow ill-posed. We will study this in more detail when we cover observers

Applying LQR Control



Application #1: trajectory generation

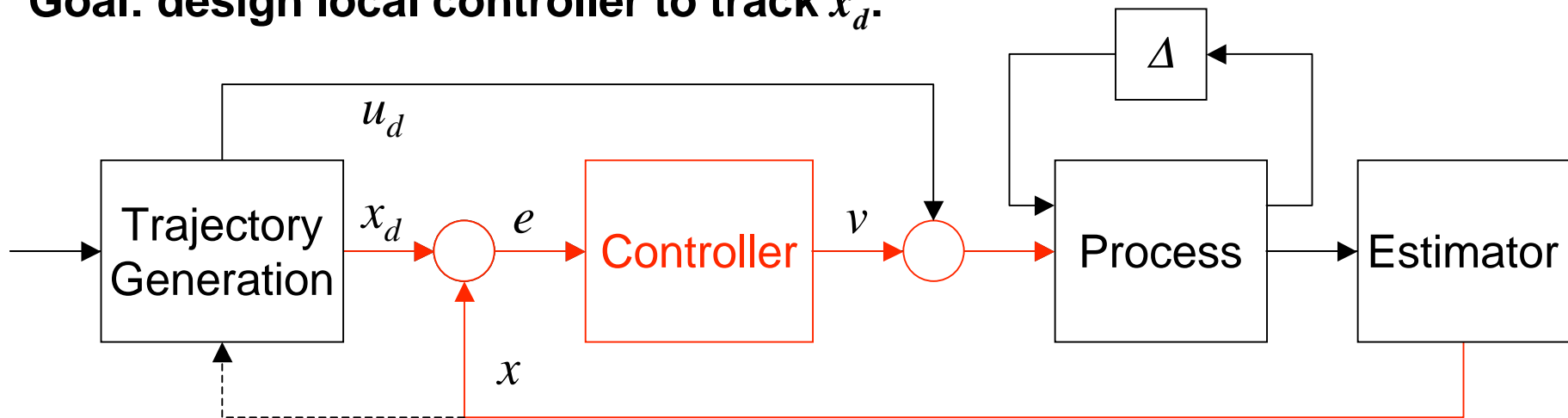
- Solve for (x_d, y_d) that minimize quadratic cost over finite horizon (requires linear process)
- Use local controller to regulate to desired trajectory

Application #2: trajectory tracking

- Solve LQR problem to stabilize the system to the origin \Rightarrow feedback $u = Kx$
- Can use this for local stabilization of *any* desired trajectory
- Missing: so far, have assumed we want to keep x small (versus $x \rightarrow x_d$)

LQR for trajectory tracking

Goal: design local controller to track x_d :



Approach: regulate the *error dynamics*

- Let $e = x - x_d$, $v = u - u_d$ and assume $f(x, u) = f(x) + g(x)u$ (simplifies notation)

$$\begin{aligned}\dot{e} &= \dot{x} - \dot{x}_d = f(x) + g(x)u - f(x_d) + g(x_d)u_d \\ &= f(e + x_d) - f(x_d) + g(e + x_d)(v + u_d) - g(x_d)u_d \\ &= F(e, v, x_d(t), u_d(t))\end{aligned}$$

- Now linearize the dynamics around $e = 0$ and design controller $v = K e$
- Final control law will be $u = K(x - x_d) + u_d$
- Note: in general, linearization will depend on $x_d \Rightarrow u = K(x_d)x \leftarrow$ “gain scheduling”

Choosing LQR weights

Most common case: diagonal weights

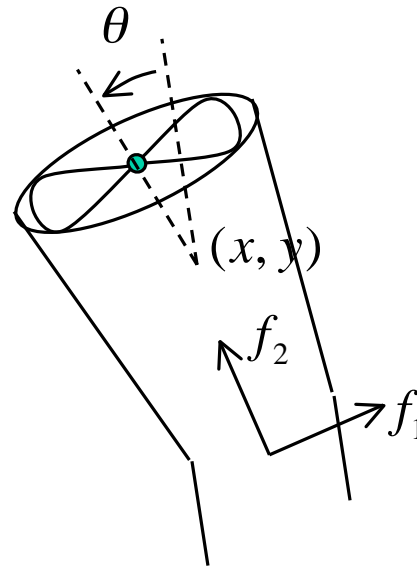
$$Q = \begin{bmatrix} q_1 & & \\ & \cdots & \\ & & q_n \end{bmatrix} \quad R = \rho \begin{bmatrix} r_1 & & \\ & \cdots & \\ & & r_n \end{bmatrix}$$

- Weight each state/input according to how much it contributes to cost
- Eg: if error in x_1 is 10x as bad as error in x_2 , then $q_1 = 10 q_2$
- OK to set some state weights to zero, but *all* input weights must be > 0
- Remember to take units into account: eg for ducted fan if position error is in meters and pitch error is in radians, weights will have different “units”

Remarks

- LQR will *always* give a stabilizing controller, but no guaranteed margins
- LQR shifts design problem from loop shaping to weight choices
- Most practical design uses LQR as a first cut, and then tune based on system performance

Example: Ducted Fan



Stabilization:

- Given an equilibrium position (x_d, y_d) and equilibrium thrust f_{2d} , maintain stable hover
- Full state available for feedback

Tracking:

- Given a reference trajectory $(x_r(t), y_r(t))$, find a feasible trajectory \vec{x}_d, u_d and a controller $u = \alpha(x, x_d, u_d)$ such that $x \rightarrow x_d$

Equations of motion

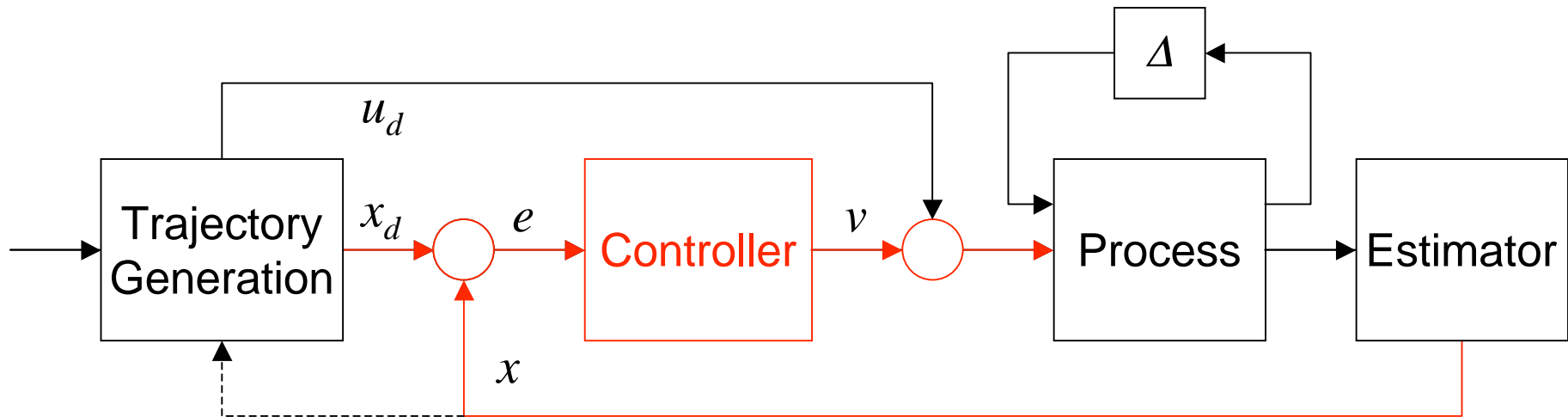
$$m\ddot{x} = f_1 \cos \theta - f_2 \sin \theta - c_{d,x}(\theta, \dot{x})$$

$$m\ddot{y} = f_1 \sin \theta + f_2 \cos \theta - mg - c_{d,y}(\theta, \dot{y})$$

$$J\ddot{\theta} = r f_1 - mgl \sin \theta - c_{d,\theta}(\theta, \dot{\theta})$$

LQR design: see `lqr_dfan.m` (available on course web page)

Variation: Integral Action



Limitation in LQR control: perfect tracking requires perfect model

- Control law is $u = K(x - x_d) + u_d \Rightarrow u_d$ must be perfect to hold $e = 0$
- Alternative: use integral feedback to give zero steady state error

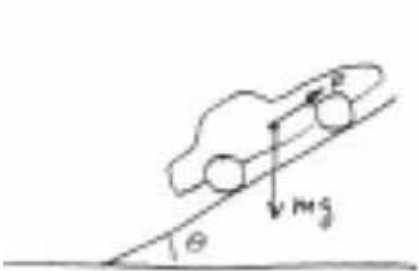
$$\frac{d}{dt} \begin{bmatrix} x \\ z \end{bmatrix} = \begin{bmatrix} Ax + Bu \\ y - r \end{bmatrix} = \begin{bmatrix} Ax + Bu \\ Cx - r \end{bmatrix} \leftarrow \text{integral of (output) error}$$

- Now design LQR controller for extended system (including integrator weight)

$$u = K(x - x_d) - K_i z + u_d$$

\leftarrow equilibrium value $\Rightarrow y = r \Rightarrow 0$ steady state error

Example: Cruise Control



$$m\dot{v} = F - F_d$$

$$F = \alpha_n u T(\alpha_n v)$$

$$F_d = mgC_r + \frac{1}{2}\rho C_v A v^2 + mg\theta,$$

Linearized around v_0 :

$$\dot{\tilde{v}} = a\tilde{v} - mg\theta + mb\tilde{u}$$

$$y = v = \tilde{v} + v_0$$

Step 1: augment linearized (error) dynamics with integrator

$$\frac{d}{dt} \begin{bmatrix} \tilde{v} \\ z \end{bmatrix} = \begin{bmatrix} \frac{a}{m} & 0 \\ -1 & 0 \end{bmatrix} \begin{bmatrix} \tilde{v} \\ z \end{bmatrix} + \begin{bmatrix} b \\ 0 \end{bmatrix} u + \begin{bmatrix} -g \\ 0 \end{bmatrix} \theta + \begin{bmatrix} 0 \\ r - v_0 \end{bmatrix}$$

Step 2: choose LQR weights and compute LQR gains

$$Q = \begin{bmatrix} q_1 & 0 \\ 0 & q_2 \end{bmatrix} \quad R = \rho \quad \rightarrow \quad K = \begin{bmatrix} k_1 & k_2 \end{bmatrix}$$

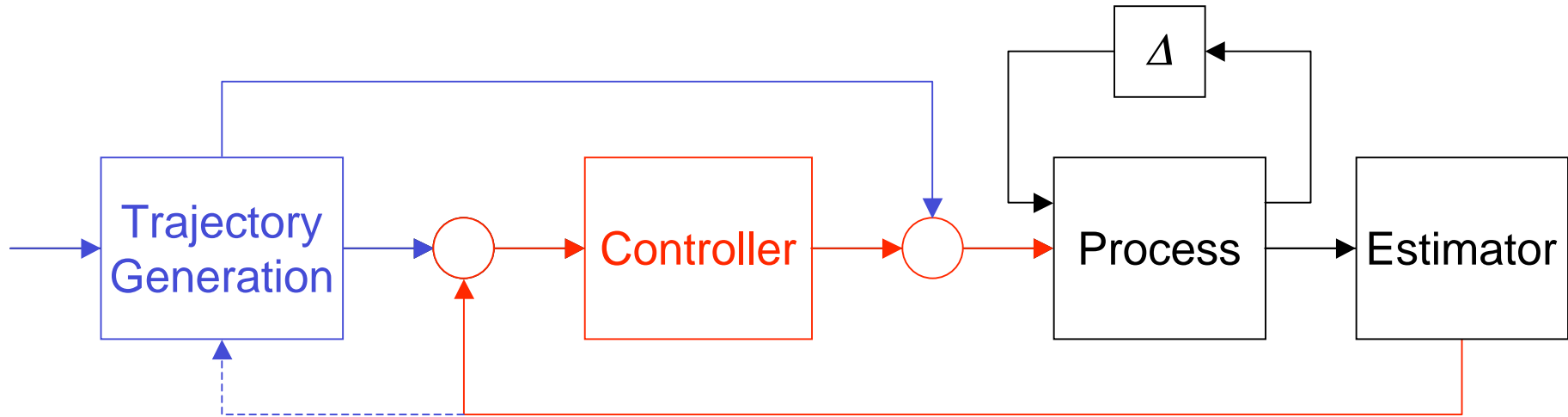
Note: linearized about v_0 but try to maintain speed r (near v_0)

Step 3: implement controller

$$\dot{z} = v - r$$

$$u = u_0 + k_1(v - r) + k_2 z \quad \leftarrow \text{PI controller}$$

Summary: LQR Control



Application #1: trajectory generation

- Solve for (x_d, y_d) that minimize quadratic cost over finite horizon
- Use local controller to track trajectory

$$J = \frac{1}{2} \int_0^T (x^T Q x + u^T R u) dt + \frac{1}{2} x^T(T) P_1 x(T)$$

Application #2: trajectory tracking

- Solve LQR problem to stabilize the system
- Solve algebraic Riccati equation to get state gain
- Can augment to track trajectory; integral action

$$J = \int_0^\infty (x^T Q x + u^T R u) dt$$

Announcements

Mailing list

- If you didn't get e-mail about TA office hours, send email to murray@cds

Late homework policy

- No late homework with out *prior* permission
- Usually willing to give a few extra days the first time you ask
- Sickness, conferences and other unavoidable conflicts usually work

Lecture recordings

- Will be posting audio recordings of lectures (along with slides) on web site