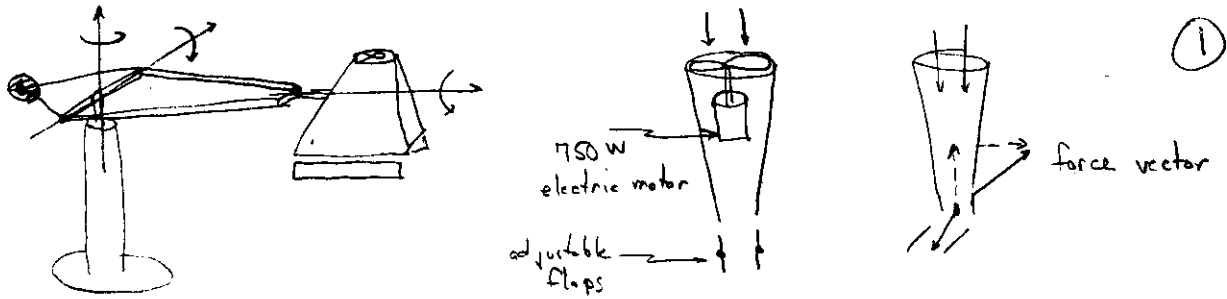


Lecture 9.2 - Control Design Example (24 Nov 04)

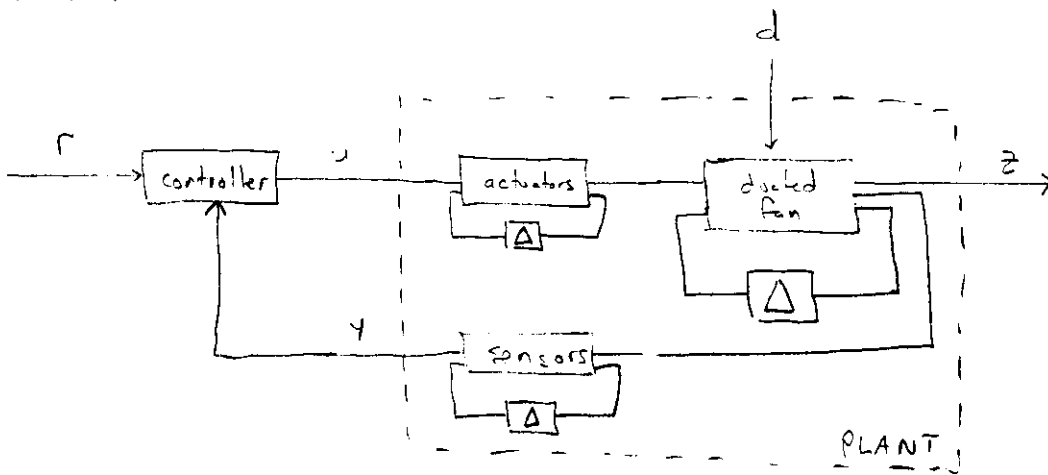
← CDS 110b update  
 RMT 19 Nov 02  
 - CDS 110a, L8.2

Example: ducted fan (vectored thrust aircraft)



Goal: track aggressive trajectories with high accuracy in presence of noise (wind), model uncertainty (variable motor dynamics, inertial parameters, etc)

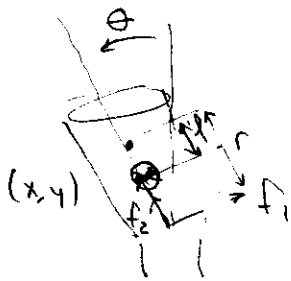
Basic picture:



$\Delta$  = unknown param  
 $d$  = disturbances  
 $z$  = regulated output

Docked Air dynamics

(2)



$$m\ddot{x} = \cos\theta f_1 - \sin\theta f_2$$

$$m\ddot{y} = \cos\theta f_2 + \sin\theta f_1 - mg$$

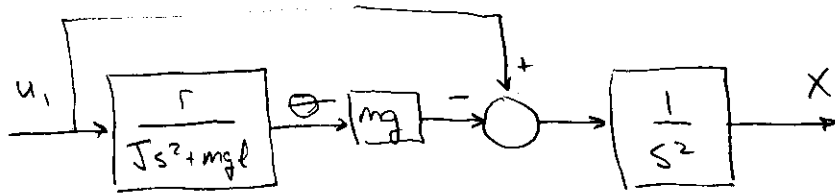
$$J\ddot{\theta} = r f_1 - mgl \sin\theta$$

Note: no damping

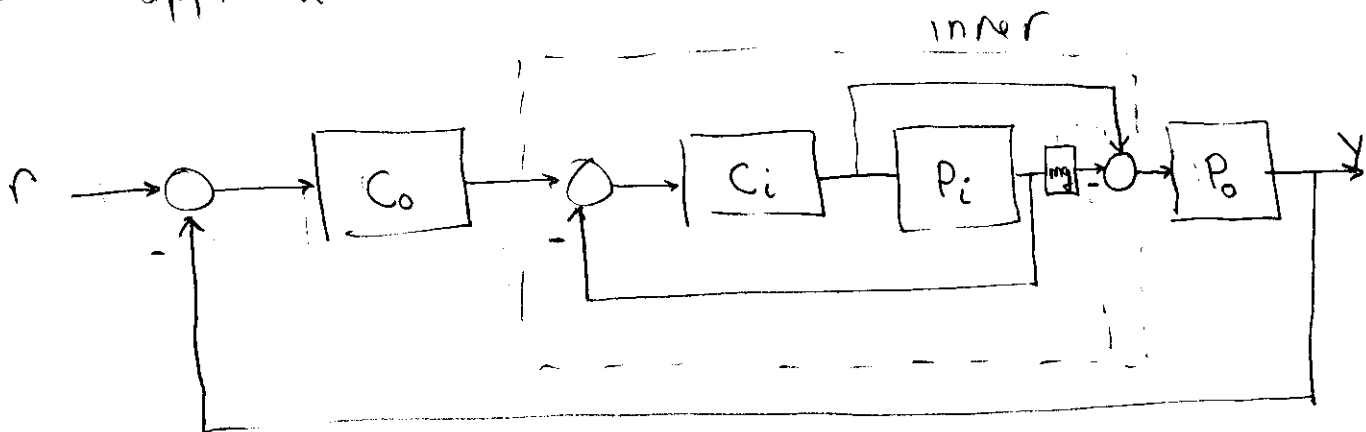
Linearize system around hover

$$\begin{matrix} x=0 & \dot{x}=0 & f_1=0 & \text{linearize} & m\ddot{x} = u_1 - mg\theta \\ y=0 & \dot{y}=0 & f_2=mg & \Rightarrow & m\ddot{y} = u_2 \\ \theta=0 & \dot{\theta}=0 & & & J\ddot{\theta} = ru_1 - mgl\theta \end{matrix}$$

Lateral dynamics:



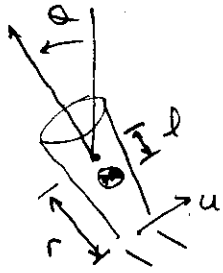
Control approach



Split design into two pieces: pitch + posn

inner      outer

Example: ducted fan pitch axis



$$\frac{\Theta(s)}{u(s)} = \frac{r}{Js^2 + mg l}$$

$r$  = flap offset, 0.25 m

$J$  = mom. of inertia, 0.047 kg m<sup>2</sup>

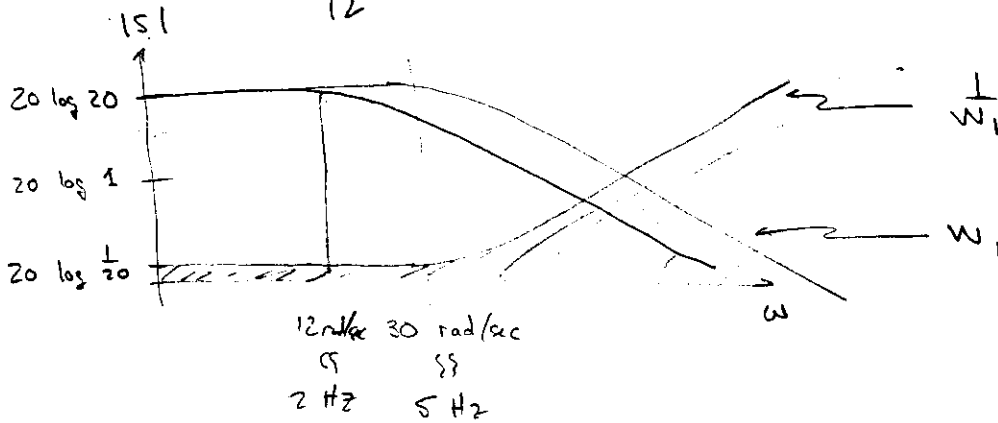
$g$  = 9.8 m/sec<sup>2</sup>

$l$  = center of mass offset, 0.05 m

$m$  = 1.5 kg

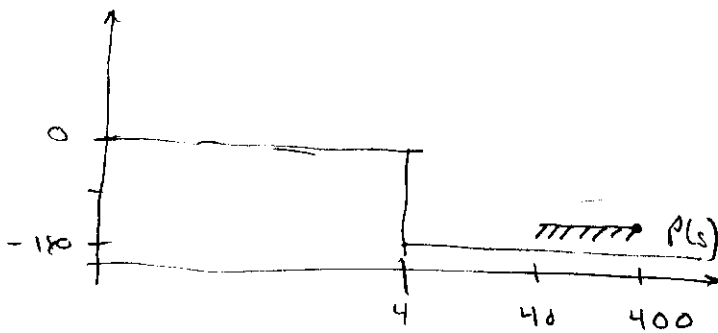
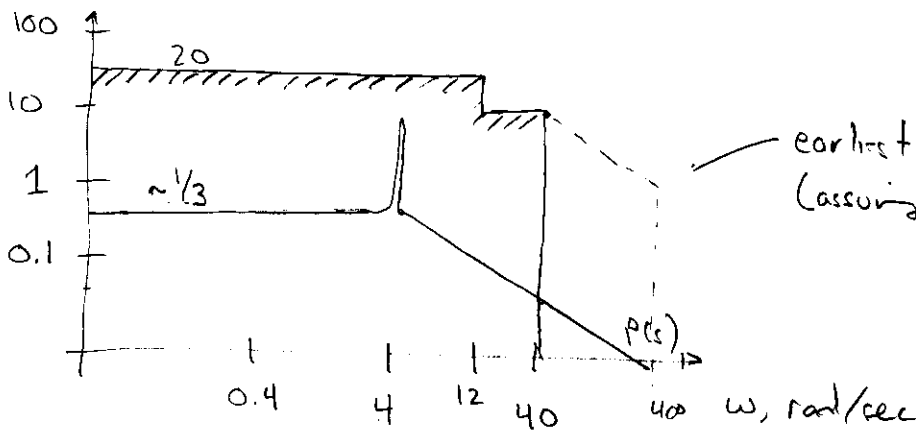
Nominal performance:  $\leq 5\%$  error up to  $\frac{2}{5}$  Hz  
 $\leq 10\%$  error up to 5 Hz

$$W_1 = \frac{20}{\left(\frac{s}{30} + 1\right)^2} \quad |W_1(s)| \leq 1 \quad s = j\omega$$



Controller design

$$P_i(s) = \frac{r}{Js^2 + mgl} \approx \frac{0.25}{0.05s^2 + 0.75} \approx \frac{5}{s^2 + 16}$$

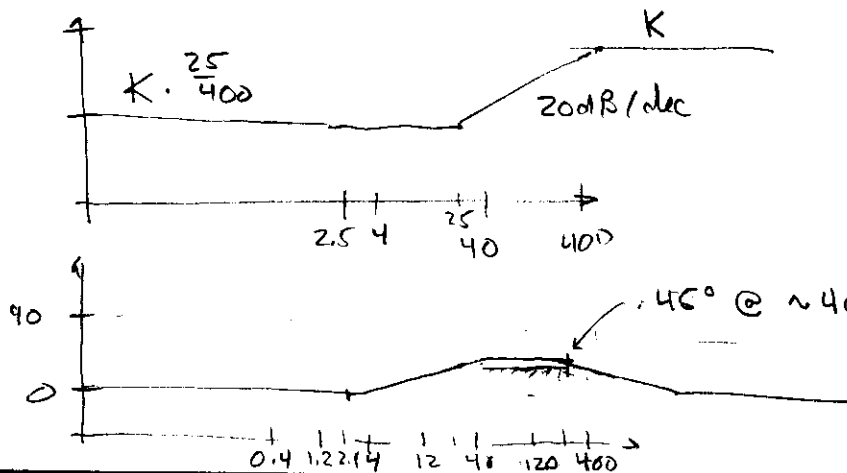


PM > 45°

Compensator design

Need to add phase lead in 40-400 Hz range

Need to add gain up to 40 Hz



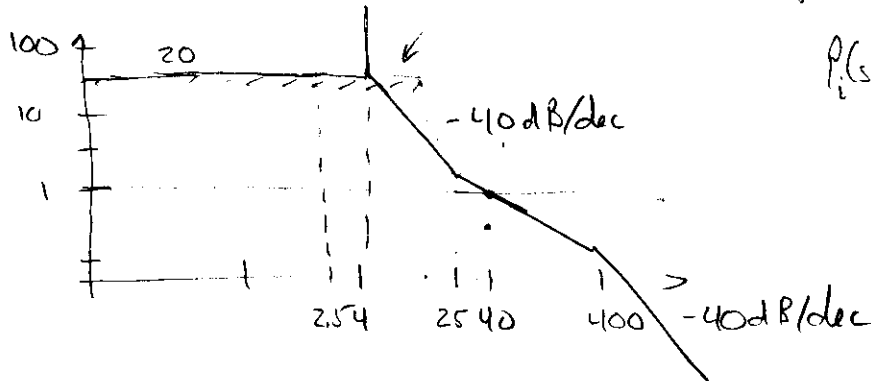
$$K \cdot \frac{25}{400} = 60 \Rightarrow K \approx 1000$$

$$C_i(s) = K \frac{s + 25}{s + 400}$$

Closed loop

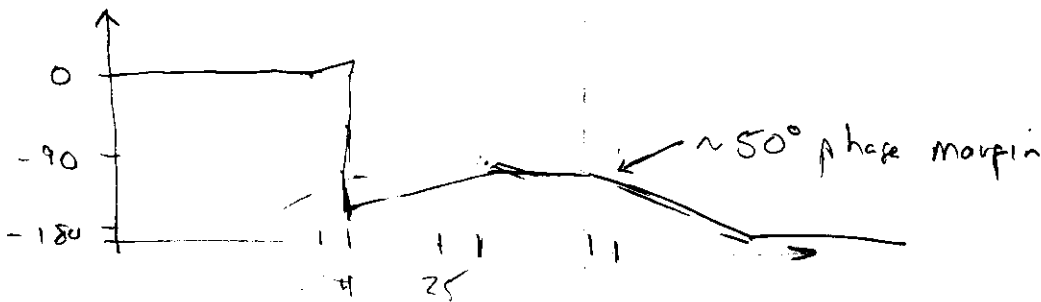
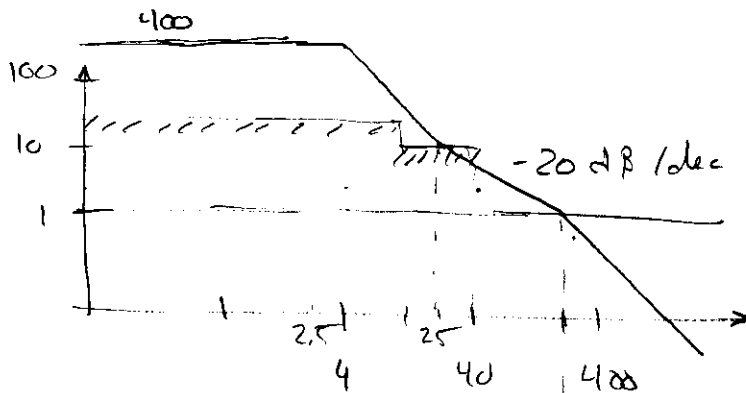
Problem: falls off too early  
 ⇒ increase gain

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$$P_i(s)G_c(s) = \frac{5}{s^2+16} \cdot \frac{1000(s+25)}{s+400}$$

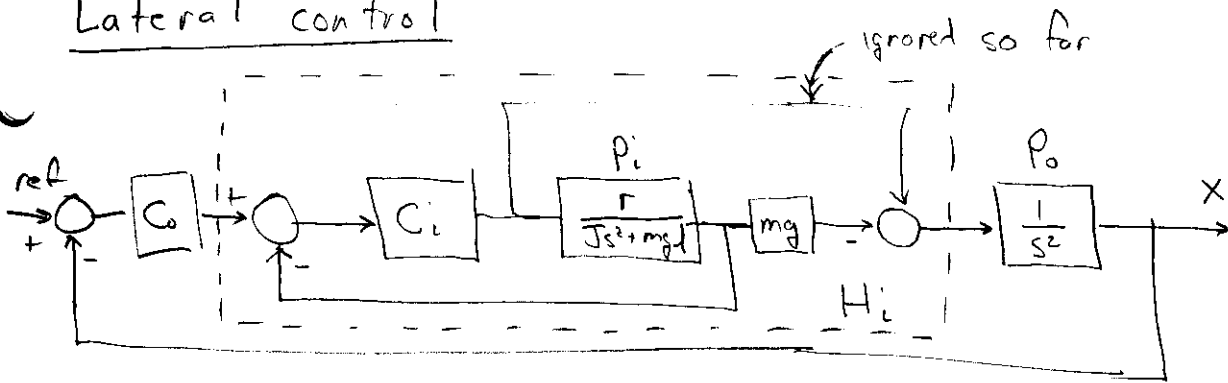
Add factor of 20 gain



warning: very low phase here.  
 ⇒ probably move back zero a bit

check:  $|W_1 S_i| < 1$  ✓  
 $|W_2 T_c| < 1$  ✓

Lateral control



Pretend that pitch controller is perfect  $\Rightarrow$  control  $\Theta$  directly

$$m\ddot{x} = u_1 - mg\Theta$$

$$J\ddot{\Theta} = ru_1 - mgd\Theta \rightarrow \Theta_d \text{ given}$$

$$SS \ u_1 = \Theta_d \frac{mgd}{r} = 0.2 mg \cdot \Theta_d$$

So, in steady state we can assume

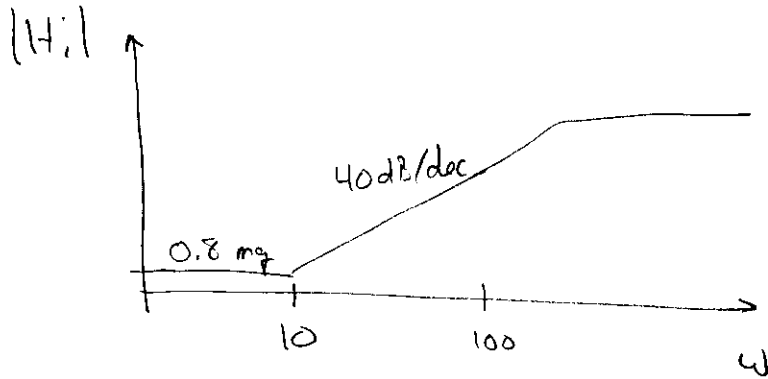
$$m\ddot{x} = (0.2 mg - mg)\Theta_d = \underline{-0.8 mg \Theta_d}$$

$v_1 \leftarrow$  pretend we control this

Q: How good an approximation is this?

A: Look at  $H_i$

$$H_i = \frac{C_i}{1 + C_i P_i} - mg \frac{C_i P_i}{1 + C_i P_i} = \frac{C_i (1 - mg P_i)}{1 + C_i P_i}$$

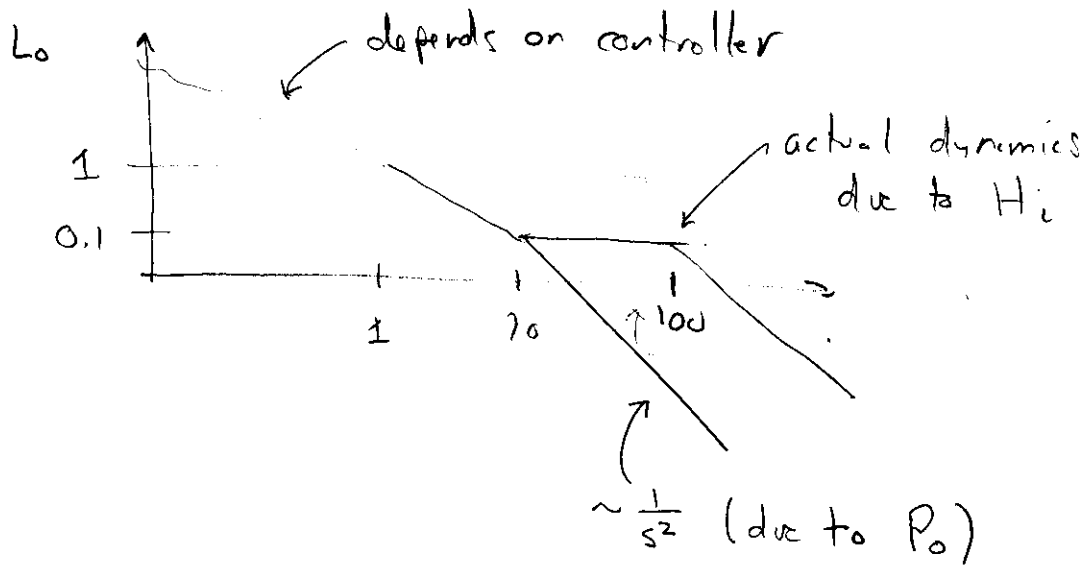
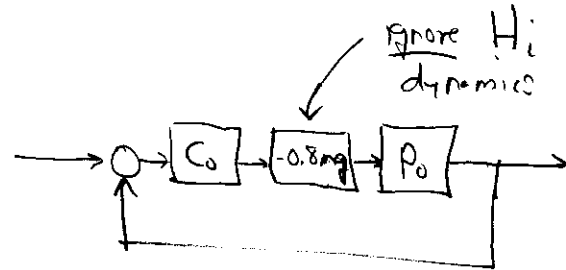


$\Rightarrow$  good approx up to  $10 \text{ rad/sec} \approx 2 \text{ Hz}$

Outer loop design goals

- 0% steady state error
- BW = 1 rad/sec
- $|L_o| < \frac{1}{10}$  for  $\omega > 10 \text{ rad/sec}$

$\Rightarrow$  roll off gain so that  $H_i$  dynamics are not a factor

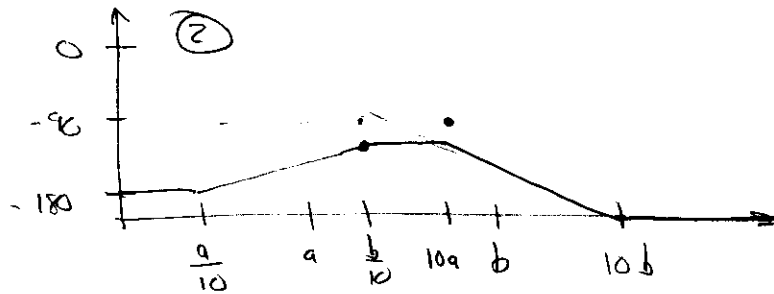
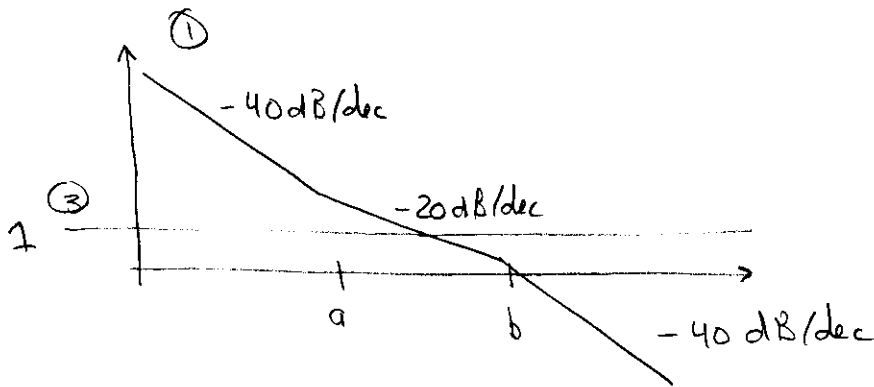


Outer loop design

$$H_2(s)P_o(s) = \frac{-0.8 \text{ mg}}{s^2}$$

$$C_o(s) = -K_o \frac{s+a_o}{s+b_o}$$

↑ to get sign of gain correct



Choose crossover at  $\sim \frac{b}{10} = 1 \text{ rad/sec} \Rightarrow b = 10$

Choose zero at  $\frac{b}{10} < 10a < b \Rightarrow \frac{1}{10} < a < 1$

Try  $a = 0.3$

Set gain at  $\omega_c = \frac{b}{10}$  to give  $|H_2(s)P_o(s)(j\omega_c)C(j\omega_c)| = 1$

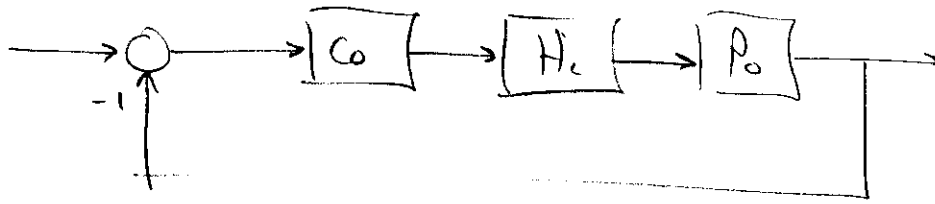
$$+ 0.8 \text{ mg} \cdot \frac{1}{1} \cdot K_o \left| \frac{j+0.3}{j+10} \right| = 1 \Rightarrow K_o = 0.8$$



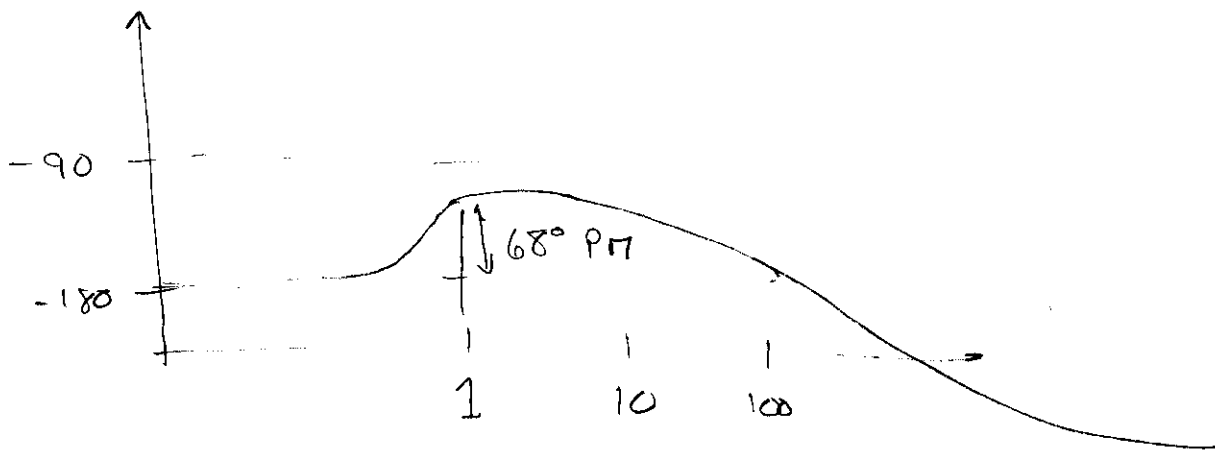
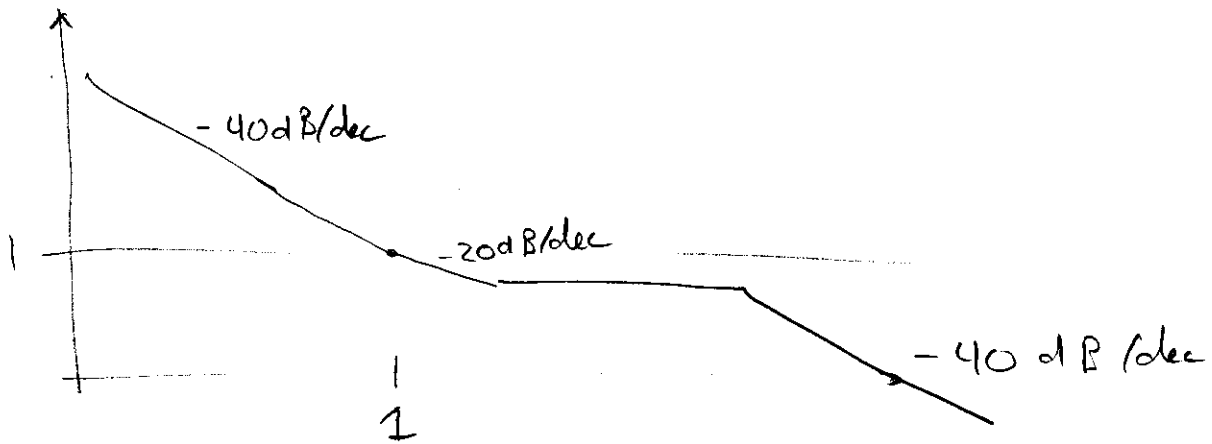
# Final design check

RM01 19 Nov 02

(10)



$$\tilde{L}_0 = C_0 H_c P_0$$



Use Nyquist to verify stability

Poles:  $-194 \pm 216j$ ,  $-11.41$ ,  $-10$ ,  $-0.51 \pm 0.23j$

Zeros:  $7.94$ ,  $-10$ ,  $-7.96$ ,  $-0.3$

Note: some PE cancellations in MATLAB