



CDS 101: Lecture 7.1 Loop Analysis of Feedback Systems



Richard M. Murray
10 November 2003

Goals:

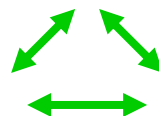
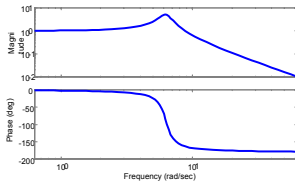
- Show how to compute closed loop stability from open loop properties
- Describe the Nyquist stability criterion for stability of feedback systems
- Define gain and phase margin and determine it from Nyquist and Bode plots

Reading:

- Åström and Murray, *Analysis and Design of Feedback Systems*, Ch 7
- *Advanced:* Lewis, Chapter 7

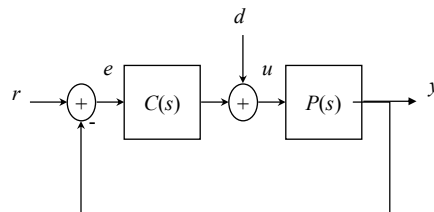
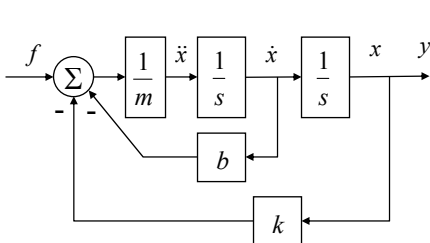
Review from Last Week

$$u = A \sin(\omega t) \rightarrow \begin{cases} \dot{x} = Ax + Bu \\ y = Cx + Du \\ x(0) = 0 \end{cases} \rightarrow y_{ss} = |H(j\omega)| A \cdot \sin(\omega t + \angle H(j\omega))$$



$$H(s) = C(sI - A)^{-1} B + D$$

$$H_{y_2 u_1} = H_{y_2 u_2} H_{y_1 u_1} = \frac{n_1 n_2}{d_1 d_2}$$



3 Nov 03

RMM and HM, Caltech CDS

0

Closed Loop Stability

Q: how do open loop dynamics affect the closed loop stability?

- Given open loop transfer function $C(s)P(s)$ determine when system is stable

Brute force answer: compute poles closed loop transfer function

$$H_{yr} = \frac{PC}{1+PC} = \frac{n_p n_c}{d_p d_c + n_p n_c}$$

- Poles of H_{yr} = zeros of $1 + PC$
- Easy to compute, but not so good for design

Alternative: look for conditions on PC that lead to instability

- Example: if $PC(s) = -1$ for some $s = j\omega$, then system is *not* asymptotically stable
- Condition on PC is much nicer because we can *design* $PC(s)$ by choice of $C(s)$
- However, checking $PC(s) = -1$ is not enough; need more sophisticated check

11 Nov 02
R. M. Murray, Caltech CDS
3

Game Plan: Frequency Domain Design

Goal: figure out how to *design* $C(s)$ so that $1+C(s)P(s)$ is stable *and* we get good performance

$$H_{yr} = \frac{PC}{1+PC}$$

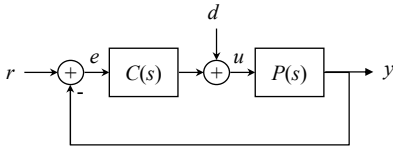
- Poles of H_{yr} = zeros of $1 + PC$
- Would also like to “shape” H_{yr} to specify performance at different frequencies

- Low frequency range:

$$PC \gg 1 \Rightarrow \frac{PC}{1+PC} \approx 1$$
 (good tracking)
- Bandwidth: frequency at which closed loop gain = $\frac{1}{2}$ \Rightarrow open loop gain ≈ 1
- Idea: use $C(s)$ to *shape* PC (under certain constraints)
- Need tools to analyze stability and performance for closed loop given PC

11 Nov 02
R. M. Murray, Caltech CDS
4

Nyquist Criterion



Determine stability from (open) loop transfer function, $L(s) = P(s)C(s)$.

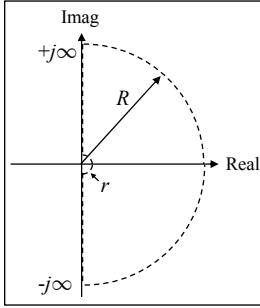
- Use "principle of the argument" from complex variable theory (see reading)

Thm (Nyquist). Consider the Nyquist plot for loop transfer function $L(s)$. Let

- P # RHP poles of $L(s)$
- N # clockwise encirclements of -1
- Z # RHP zeros of $1 + L(s)$

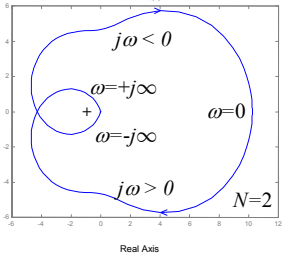
Then

$$Z = N + P$$



- Nyquist "D" contour
- Take limit as $r \rightarrow 0, R \rightarrow \infty$
- Trace from $-\infty$ to $+\infty$ along imaginary axis

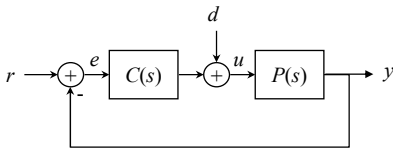
Nyquist Diagrams
From L(1)



- Trace frequency response for $L(s)$ along the Nyquist "D" contour
- Count net # of clockwise encirclements of the -1 point

11 Nov 02
R. M. Murray, Caltech CDS
5

Simple Interpretation of Nyquist

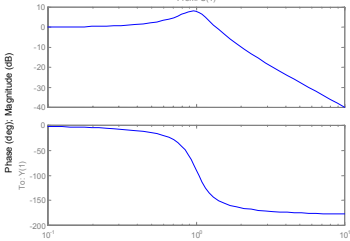


Basic idea: avoid positive feedback

- If $L(s)$ has 180° phase (or greater) and gain greater than 1, then signals are amplified around loop
- Use when phase is monotonic
- General case requires Nyquist

Can generate Nyquist plot from Bode plot + reflection around real axis

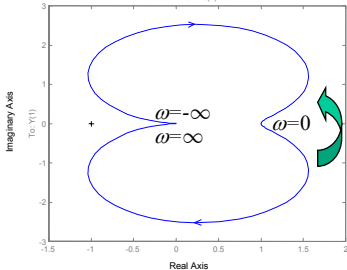
Bode Diagrams
From L(1)



bode(sys)

➔


Nyquist Diagrams
From L(1)



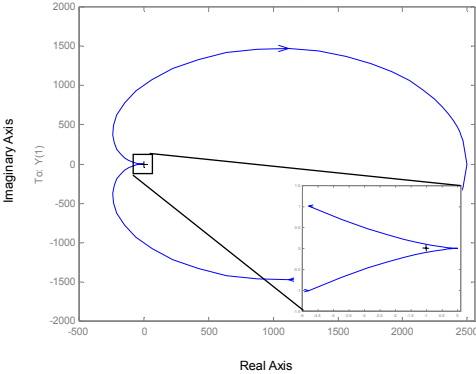
nyquist(sys)

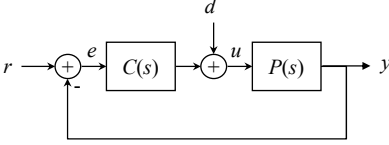
11 Nov 02
R. M. Murray, Caltech CDS
6

Example: Proportional + Integral* speed controller



Nyquist Diagrams
From: U(1)





$$P(s) = \frac{1/m}{s + b/m} \cdot \frac{r}{s + a}$$

$$C(s) = K_p + \frac{K_i}{s + 0.01}$$

Remarks

- $N = 0, P = 0 \Rightarrow Z = 0$ (stable)
- Need to zoom in to make sure there are no net encirclements
- Note that we don't have to compute closed loop response

* slightly modified; more on the design of this compensator in next week's lecture

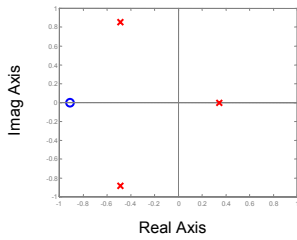
11 Nov 02
R. M. Murray, Caltech CDS
7

More complicated systems

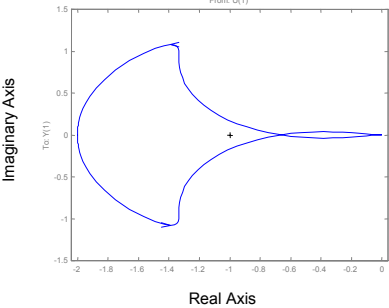
What happens when open loop plant has RHP poles?

- $1 + PC$ has singularities inside D contour \Rightarrow these must be taken into account

Pole-zero map



Nyquist Diagrams
From: U(1)



$$L(s) = \frac{s + 1}{s - 0.5} \cdot \frac{1}{s^2 + s + 1}$$

unstable pole \nearrow

$$\frac{1}{1 + L} = \frac{s + 1}{(s + 0.35)(s + 0.07 + 1.2j)(s + 0.07 - 1.2j)} \checkmark$$

$N = -1, P = 1 \Rightarrow Z = N + P = 0$ (stable)

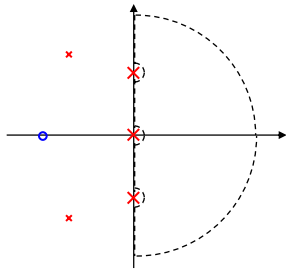
11 Nov 02
R. M. Murray, Caltech CDS
8

Comments and cautions

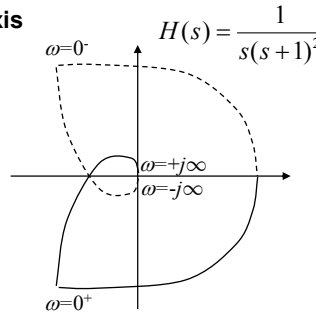
Why is the Nyquist plot *useful*?

- Old answer: easy way to compute stability (before computers and MATLAB)
- Real answer: gives *insight* into stability and robustness; very useful for reasoning about stability

Nyquist plots for systems with poles on the $j\omega$ axis



- chose contour to avoid poles on axis
- need to carefully compute Nyquist plot at these points
- evaluate $H(\epsilon+0j)$ to determine direction



Cautions with using MATLAB

- MATLAB doesn't generate portion of plot for poles on imaginary axis
- These must be drawn in by hand (make sure to get the orientation right!)

11 Nov 02

R. M. Murray, Caltech CDS

9

Relative stability: gain and phase margins

Nyquist plot tells us if closed loop is stable, but not *how* stable

Gain margin

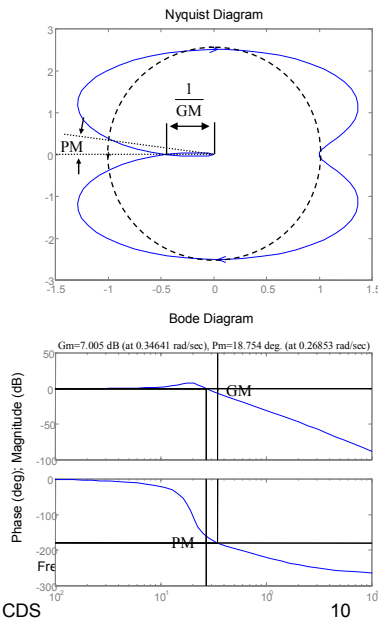
- How much we can modify the *loop gain* and still have the system be stable
- Determined by the location where the loop transfer function crosses 180° phase

Phase margin

- How much we can add “phase delay” and still have the system be stable
- Determined by the phase at which the loop transfer function has unity gain

Bode plot interpretation


- Look for gain = 1, 180° phase crossings
- MATLAB: margin(sys)

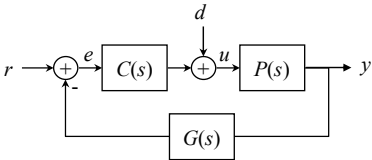


11 Nov 02

R. M. Murray, Caltech CDS

Example: cruise control





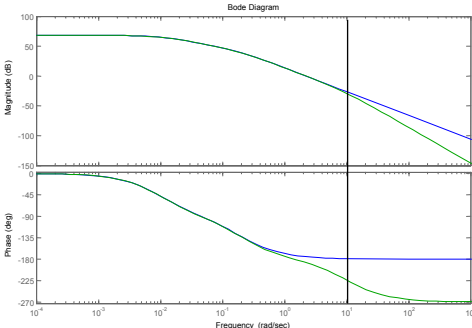
$$P(s) = \frac{1/m}{s + b/m} \cdot \frac{r}{s + a}$$

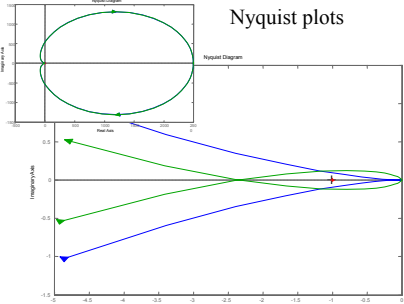
$$C(s) = K_p + \frac{K_i}{s + 0.01}$$

$$G(s) = \frac{10}{s + 10}$$

Effect of additional sensor dynamics


- New speedometer has pole at $s = 10$ (very fast); problems develop in the field
- What's the problem? A: insufficient phase margin in original design (not robust)

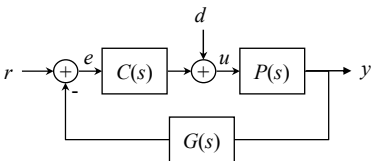




11 Nov 02
R. M. Murray, Caltech CDS
11

Preview: control design





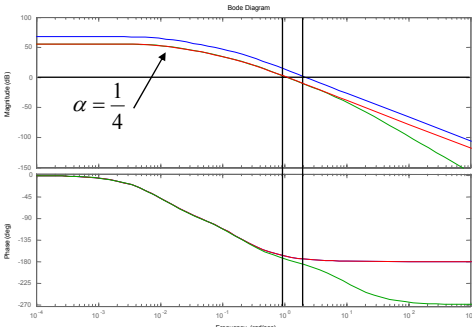
$$P(s) = \frac{1/m}{s + b/m} \cdot \frac{r}{s + a}$$

$$C(s) = \alpha \left(K_p + \frac{K_i}{s + 0.01} \right)$$

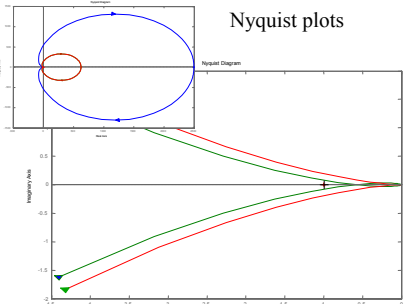
$$G(s) = \frac{10}{s + 10}$$

Approach: Increase phase margin

- Increase phase margin by reducing gain \Rightarrow can accommodate new sensor dynamics
- Tradeoff: lower gain at low frequencies \Rightarrow less bandwidth, larger steady state error

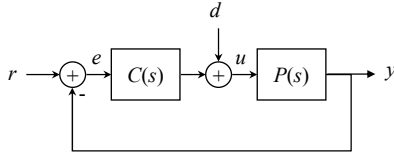


$\alpha = \frac{1}{4}$

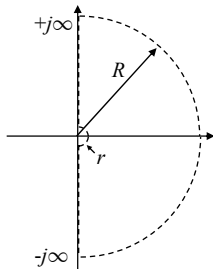


11 Nov 02
R. M. Murray, Caltech CDS
12

Summary: Loop Analysis of Feedback Systems

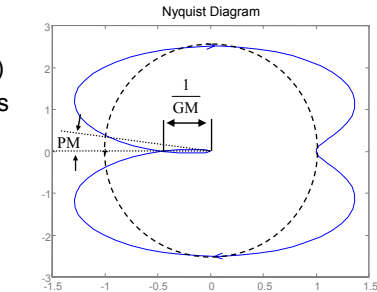
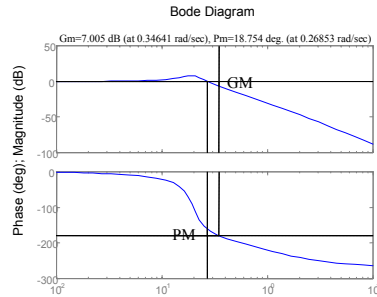


- Nyquist criteria for loop stability
- Gain, phase margin for robustness



Thm (Nyquist).
 P # RHP poles of $L(s)$
 N # CW encirclements
 Z # RHP zeros

$$Z = N + P$$



11 Nov 02

R. M. Murray, Caltech CDS

13

What's Next

Homework problems

- Nyquist plots; gain, phase margins
- Cruise control design
- CDS 110: PI control + time delay

Wednesday

- Nyquist analysis
- Control of second order systems
- Time delays

Friday

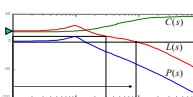
- Hideo Mabuchi, Closed-loop atomic magnetometry (quantum control)
- Friday, 2 pm, 74 JRG

Next week: PID Control

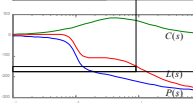
- Design of controllers using PID
- Relative stability and performance

Lecture 8.1: Frequency Domain Design

Loop Shaping for Stability and Performance
 • Steady state error, bandwidth, tracking



Main ideas
 • Performance specifications give bounds on loop transfer function
 • Use controller to shape response
 • Gain/phase relationships constrain design approach
 • Standard compensators: proportional, lead, PI



18 Nov 02

R. M. Murray, Caltech CDS

0

Don't forget to fill out MUD CARDS

11 Nov 02

R. M. Murray, Caltech CDS

14