CDS 101: Lecture 7.1
Loop Analysis of Feedback Systems

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Goals:

- Show how to compute closed loop stability from open loop properties
- Describe the Nyquist stability criterion for stability of feedback systems
- Define gain and phase margin and determine it from Nyquist and Bode plots

Reading:

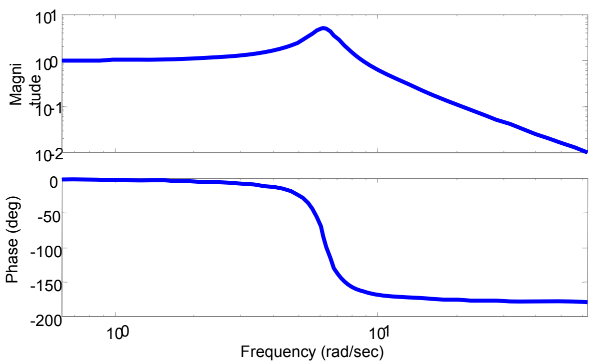
- Åström and Murray, *Analysis and Design of Feedback Systems,* Ch 7

Review from Last Week

$$u = A\sin(\omega t)$$

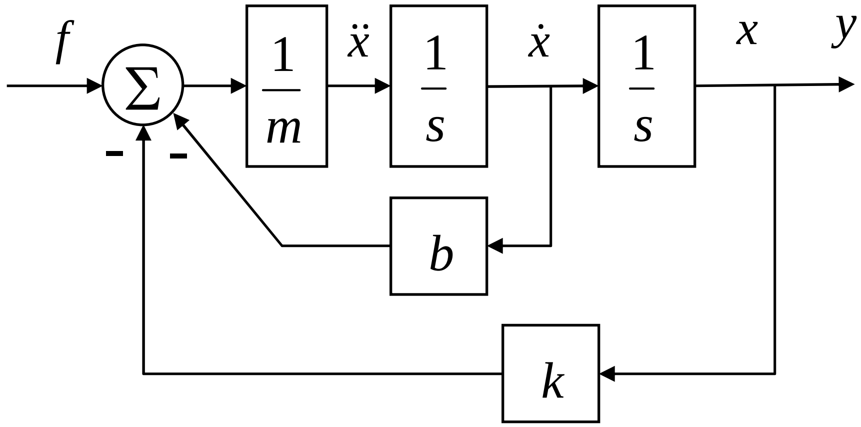
$$\dot{x} = Ax + Bu$$
$$y = Cx + Du$$
$$x(0) = 0$$

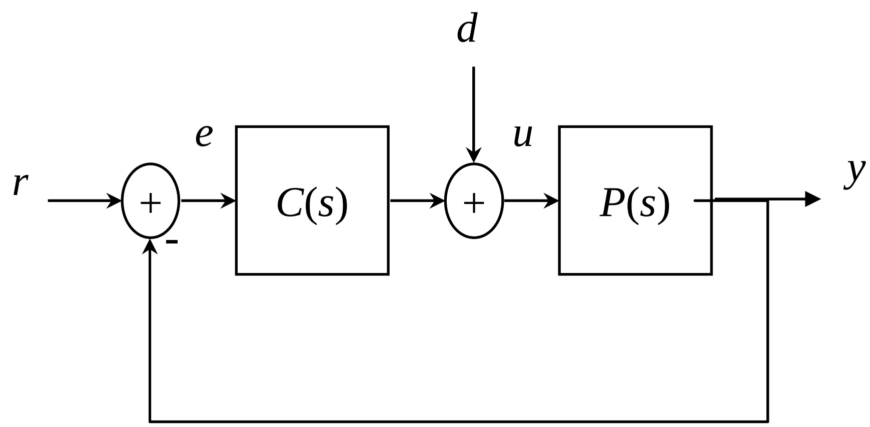
$$y_{ss} = |H(j\omega)|A \cdot \sin\left(\omega t + \angle H(j\omega)\right)$$



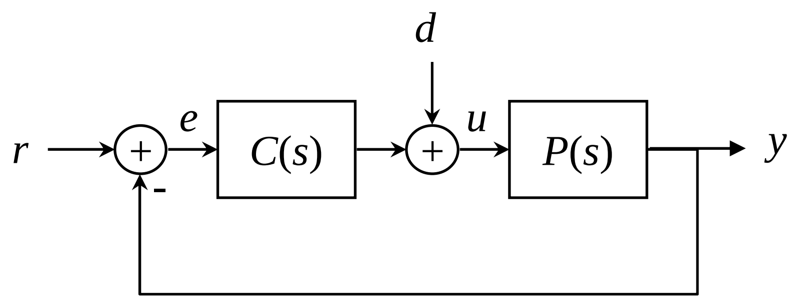
$$H(s) = C(sI - A)^{-1}B + D$$

$$H_{y_2 u_1} = H_{y_2 u_2} H_{y_1 u_1} = \frac{n_1 n_2}{d_1 d_2}$$





Closed Loop Stability



Q: how do open loop dynamics affect the closed loop stability?

- Given open loop transfer function $C(s)P(s)$ determine when system is stable

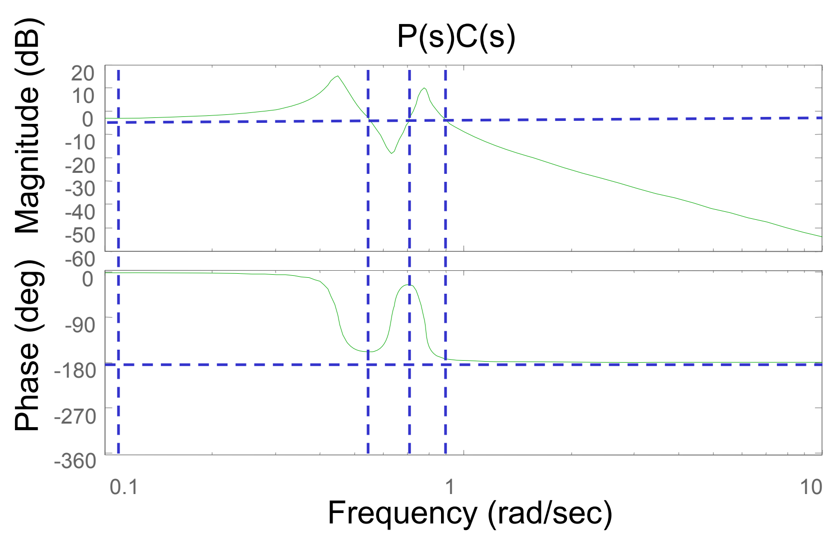
Brute force answer: compute poles closed loop transfer function

$$H_{yr} = \frac{PC}{1+PC} = \frac{n_p n_c}{d_p d_c + n_p n_c}$$

- Poles of H_{yr} = zeros of $1 + PC$
- Easy to compute, but not so good for design

Alternative: look for conditions on *PC* that lead to instability

- Example: if *PC*(*s*) = -1 for some $s = j\omega$, then system is *not* asymptotically stable
- Condition on *PC* is much nicer because we can *design PC*(*s*) by choice of *C*(*s*)
- However, checking *PC*(*s*) = -1 is not enough; need more sophisticated check

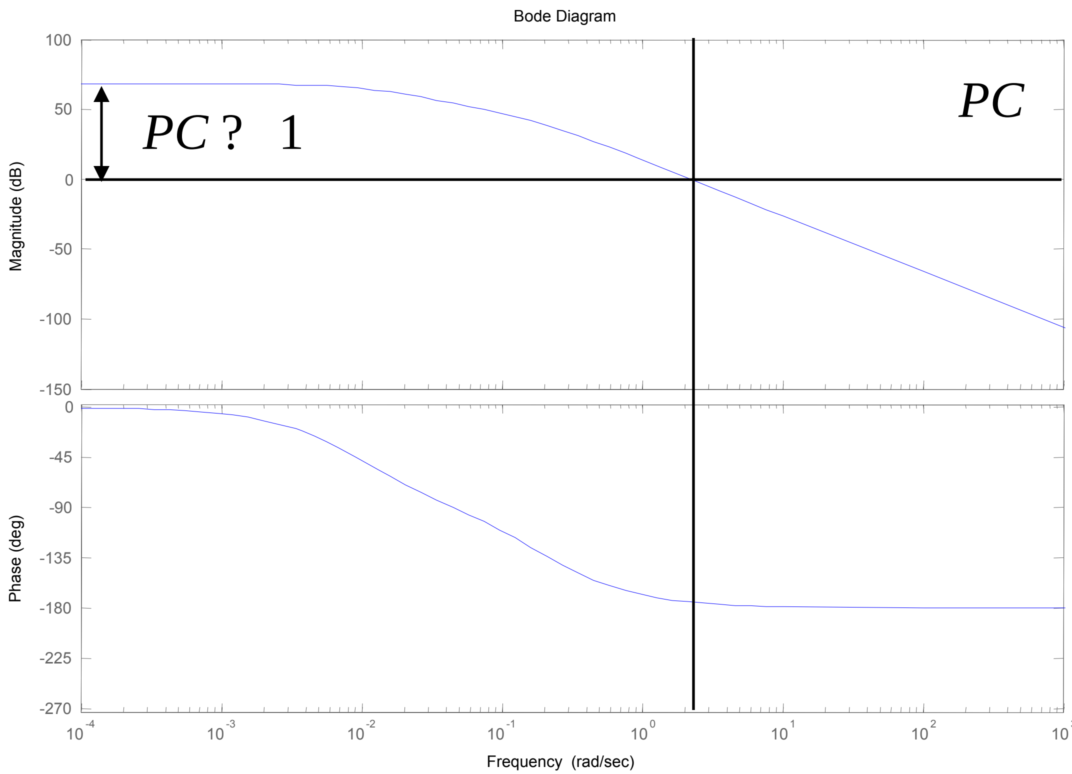


Game Plan: Frequency Domain Design

Goal: figure out how to *design* $C(s)$ so that $1+C(s)P(s)$ is stable *and* we get good performance

$$H_{yr} = \frac{PC}{1+PC}$$

- Poles of H_{yr} = zeros of 1 + PC
- Would also like to "shape" H_{yr} to specify performance at differenct frequencies

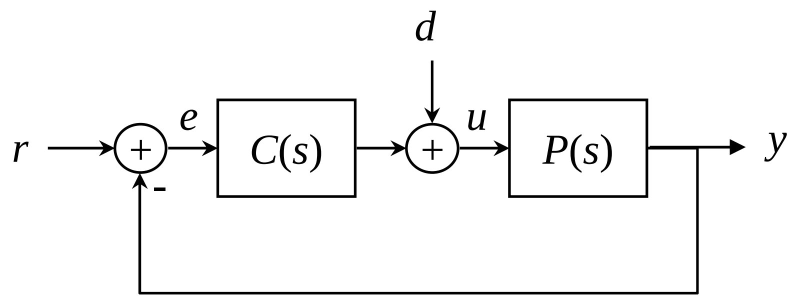


- Low frequency range:

$$PC \,?\; 1 \;\Rightarrow\; \frac{PC}{1+PC} \approx 1$$

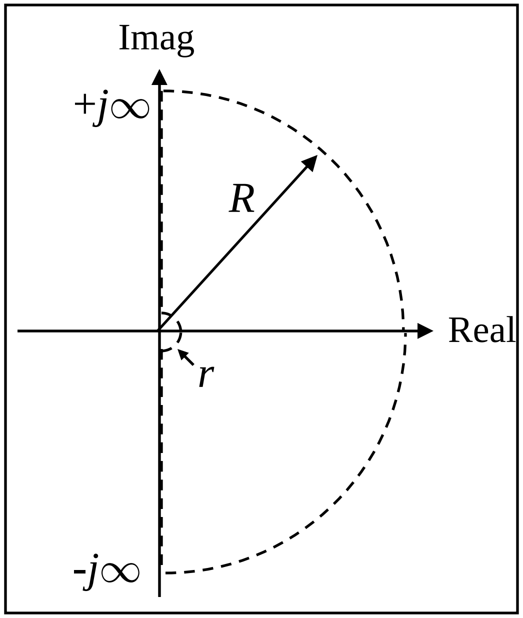
  (good tracking)
- Bandwidth: frequency at which closed loop gain = ½ ⇒ open loop gain ≈ 1
- Idea: use $C(s)$ to *shape PC* (under certain constraints)
- Need tools to analyze stability and performance for closed loop given PC

Nyquist Criterion



Determine stability from (open) loop transfer function, $L(s) = P(s)C(s)$.

- Use "principle of the argument" from complex variable theory (see reading)



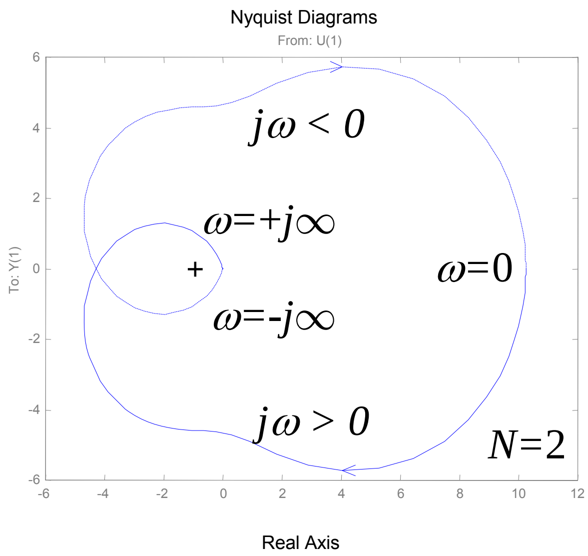
- Nyquist "D" contour
- Take limit as $r \to 0$, $R \to \infty$
- Trace from $-\infty$ to $+\infty$ along imaginary axis

Thm (Nyquist). Consider the Nyquist plot for loop transfer function $L(s)$. Let

P	# RHP poles of $L(s)$
N	# clockwise encirclements of -1
Z	# RHP zeros of $1 + L(s)$

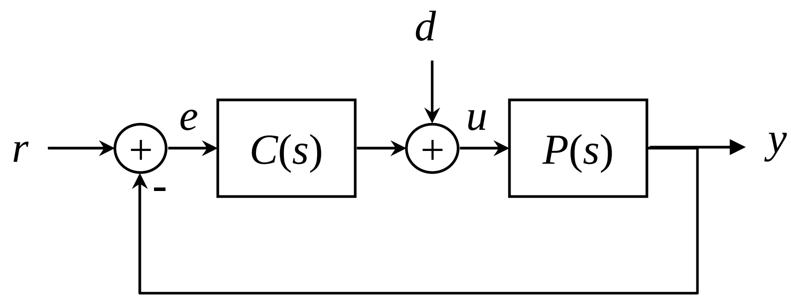
Then

$$Z = N + P$$



- Trace frequency response for $L(s)$ along the Nyquist "D" contour
- Count net # of clockwise encirclements of the -1 point

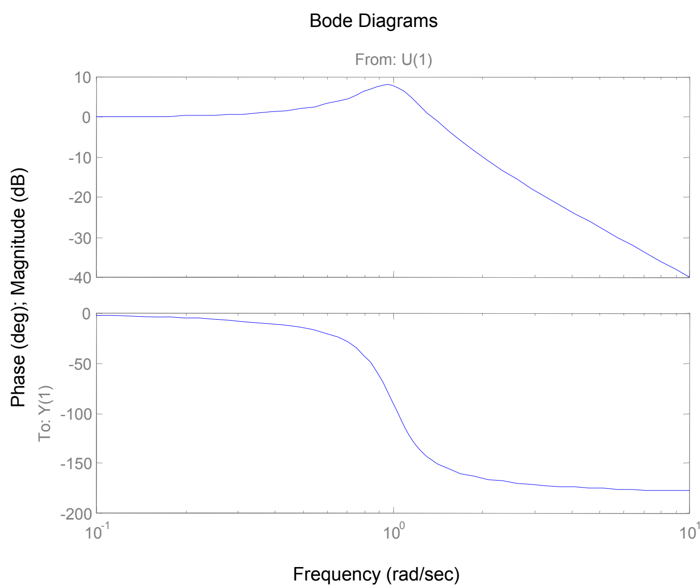
Simple Interpretation of Nyquist



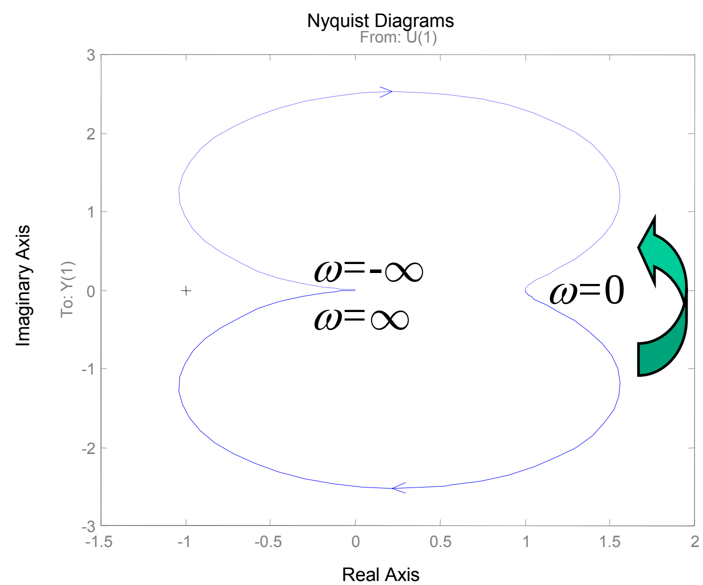
Basic idea: avoid positive feedback

- If $L(s)$ has 180° phase (or greater) and gain greater than 1, then signals are amplified around loop
- Use when phase is monotonic
- General case requires Nyquist

Can generate Nyquist plot from Bode plot + reflection around real axis

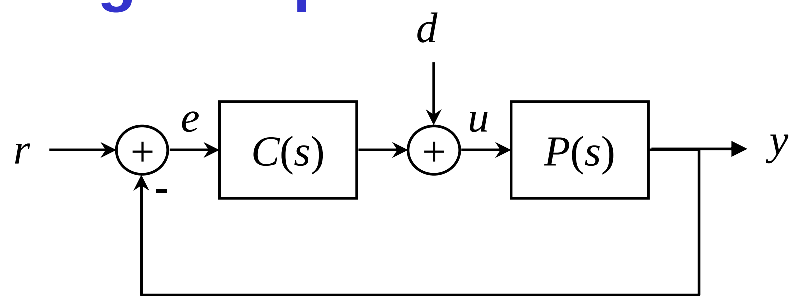


bode(sys)



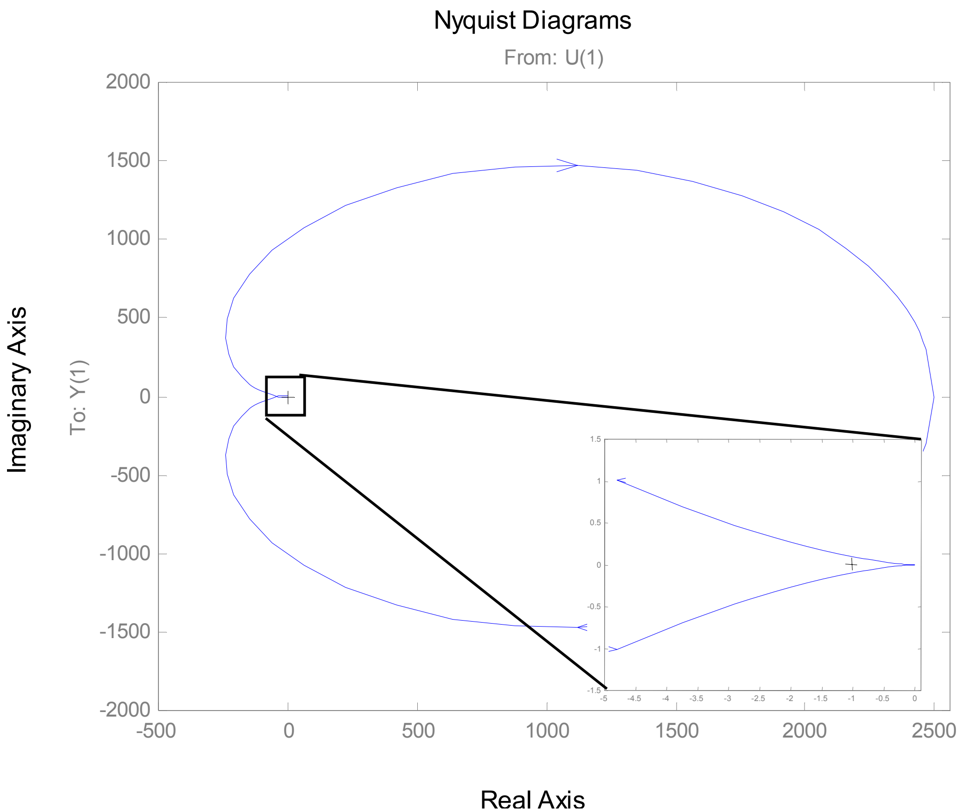
nyquist(sys)

Example: Proportional + Integral* speed controller



$$P(s) = \frac{1/m}{s + b/m} \cdot \frac{r}{s + a}$$

$$C(s) = K_p + \frac{K_i}{s + 0.01}$$



Remarks

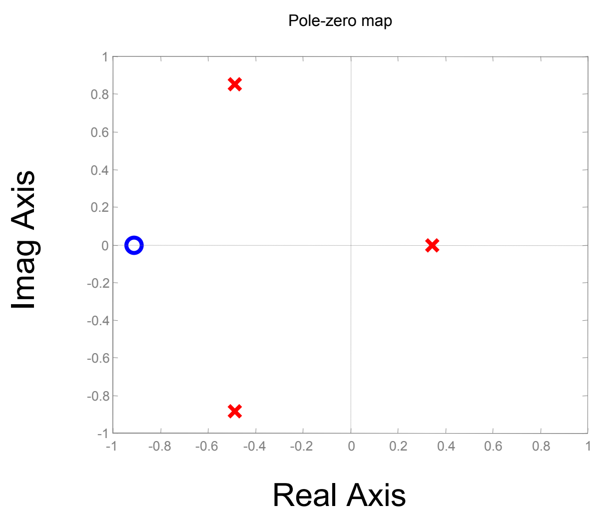
- $N = 0,\ P = 0 \Rightarrow Z = 0$ (stable)
- Need to zoom in to make sure there are no net encirclements
- Note that we don't have to compute closed loop response

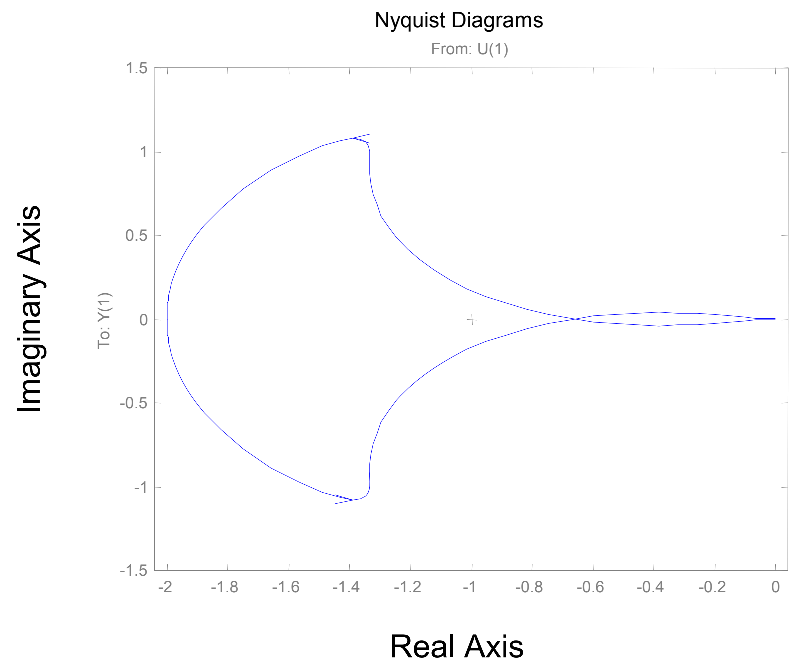
* slightly modified; more on the design of this compensator in next week's lecture

More complicated systems

What happens when open loop plant has RHP poles?

- 1 + PC has singularities inside D countour $\Rightarrow$ these must be taken into account





$$L(s) = \frac{s+1}{s-0.5} \cdot \frac{1}{s^2+s+1}$$

unstable pole

N = -1, P = 1 $\Rightarrow$ Z = N+P = 0 (stable)

$$\frac{1}{1+L} = \frac{s+1}{(s+0.35)(s+0.07+1.2j)(s+0.07-1.2j)} \checkmark$$

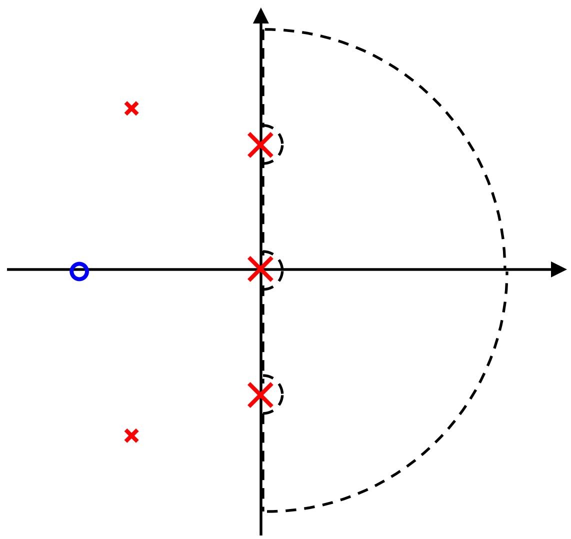
Comments and cautions

Why is the Nyquist plot *useful*?

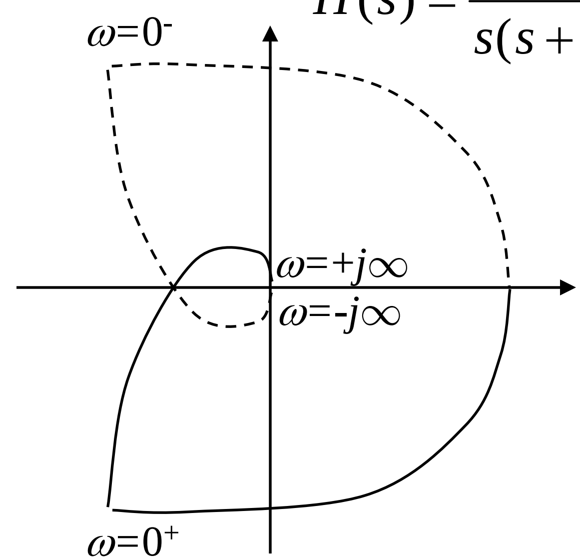
- Old answer: easy way to compute stability (before computers and MATLAB)
- Real answer: gives *insight* into stability and robustness; very useful for reasoning about stability

Nyquist plots for systems with poles on the $j\omega$ axis

$$H(s) = \frac{1}{s(s+1)^2}$$



- chose contour to avoid poles on axis
- need to carefully compute Nyquist plot at these points
- evaluate $H(\int+0j)$ to determine direction



Cautions with using MATLAB

- MATLAB doesn't generate portion of plot for poles on imaginary axis
- These must be drawn in by hand (make sure to get the orientation right!)

Robust stability: gain and phase margins

Nyquist plot tells us if closed loop is stable, but not *how* stable

Gain margin

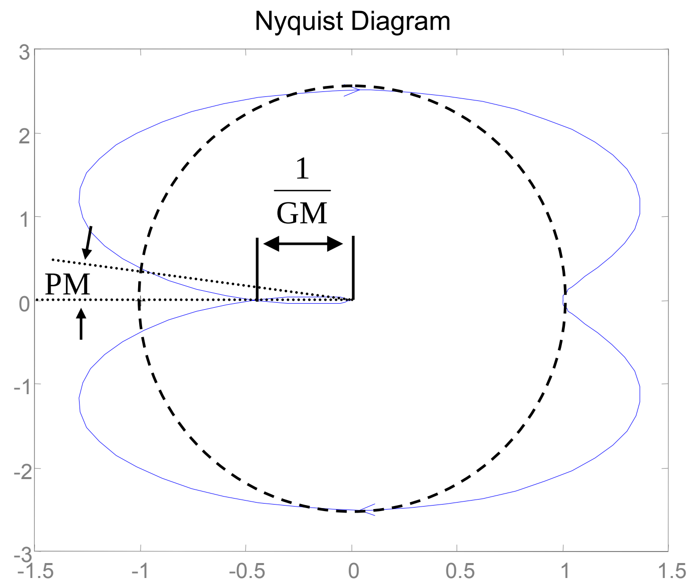
- How much we can modify the *loop gain* and still have the system be stable
- Determined by the location where the loop transfer function crosses 180˚ phase

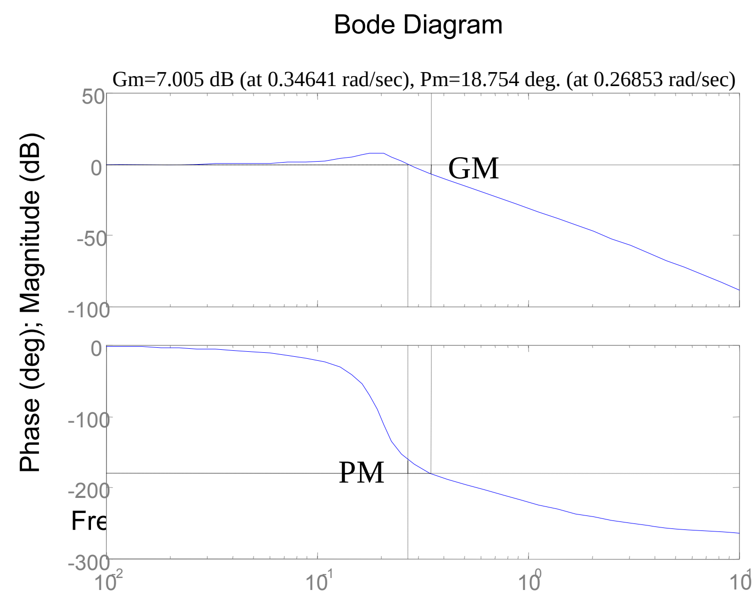
Phase margin

- How much we can add "phase delay" and still have the system be stable
- Determined by the phase at which the loop transfer function has unity gain

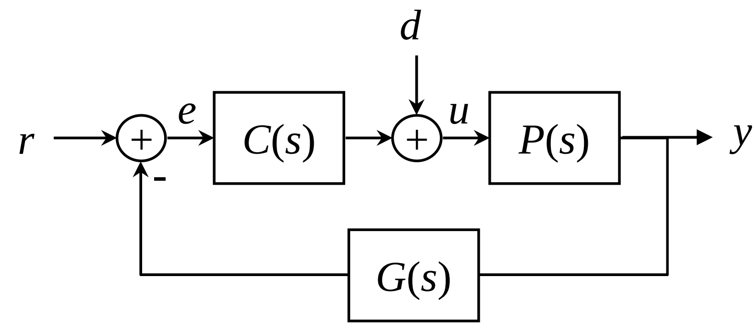
Bode plot interpretation

- Look for gain = 1, 180˚ phase crossings
- MATLAB: margin(sys)





Example: cruise control



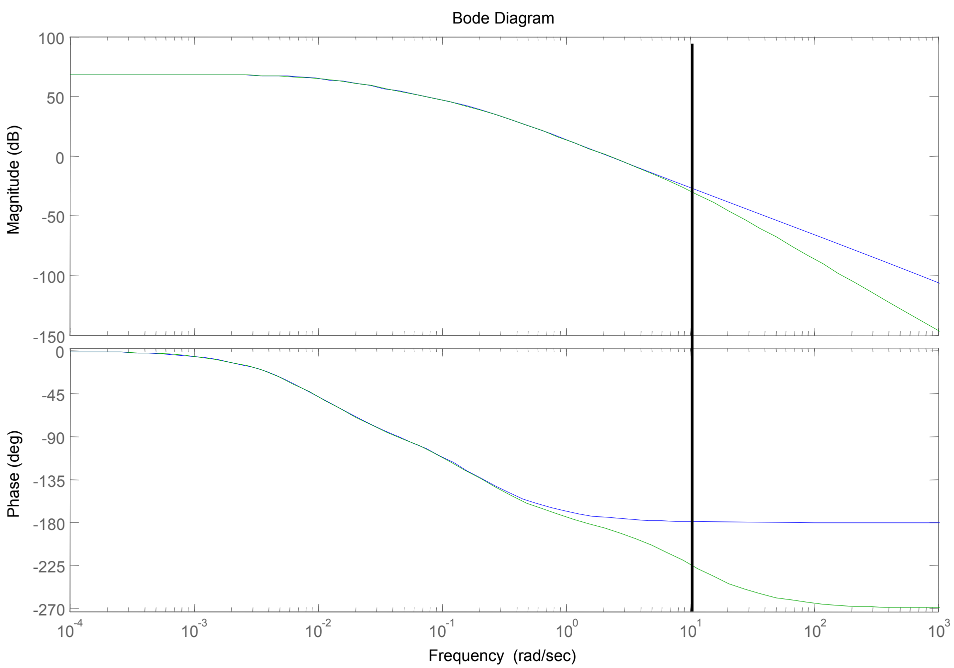
$$P(s) = \frac{1/m}{s + b/m} \cdot \frac{r}{s + a}$$

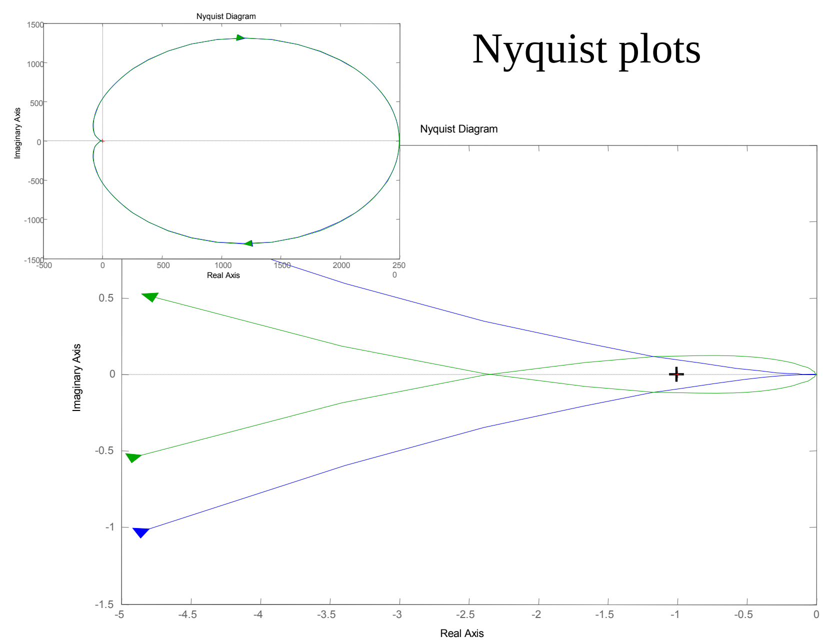
$$C(s) = K_p + \frac{K_i}{s + 0.01}$$

$$G(s) = \frac{10}{s + 10}$$

Effect of additional sensor dynamics

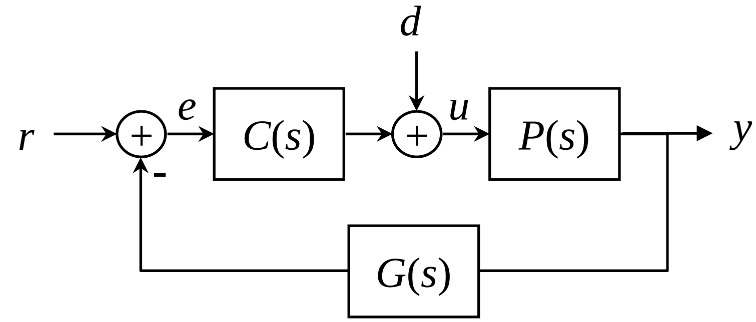
- New speedometer has pole at *s* = 10 (very fast); problems develop in the field
- What's the problem? A: insufficient phase margin in original design (not robust)





Nyquist plots

Preview: control *design*



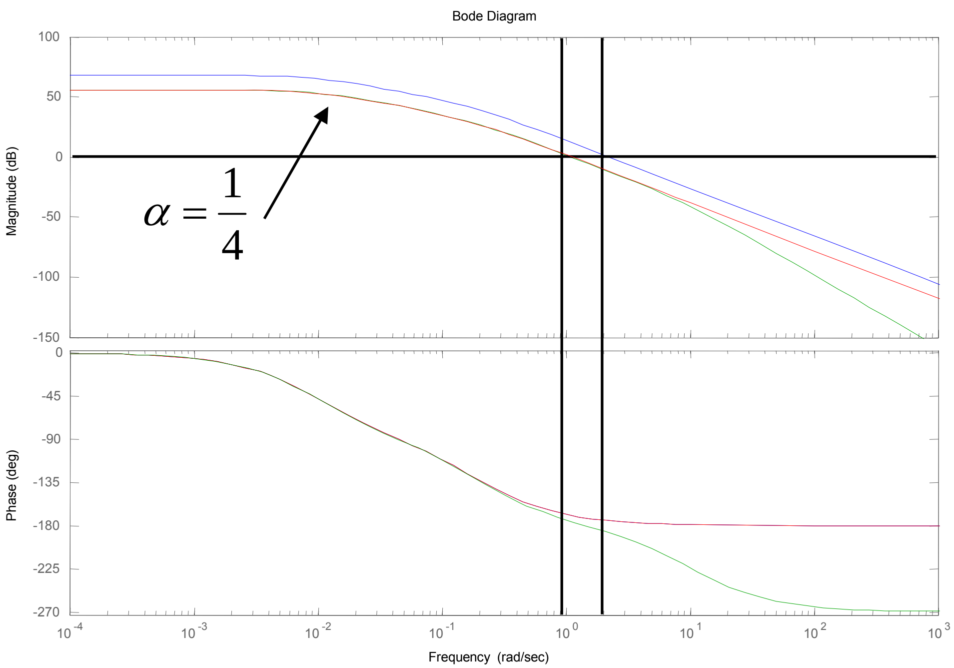
$$P(s) = \frac{1/m}{s + b/m} \cdot \frac{r}{s + a}$$

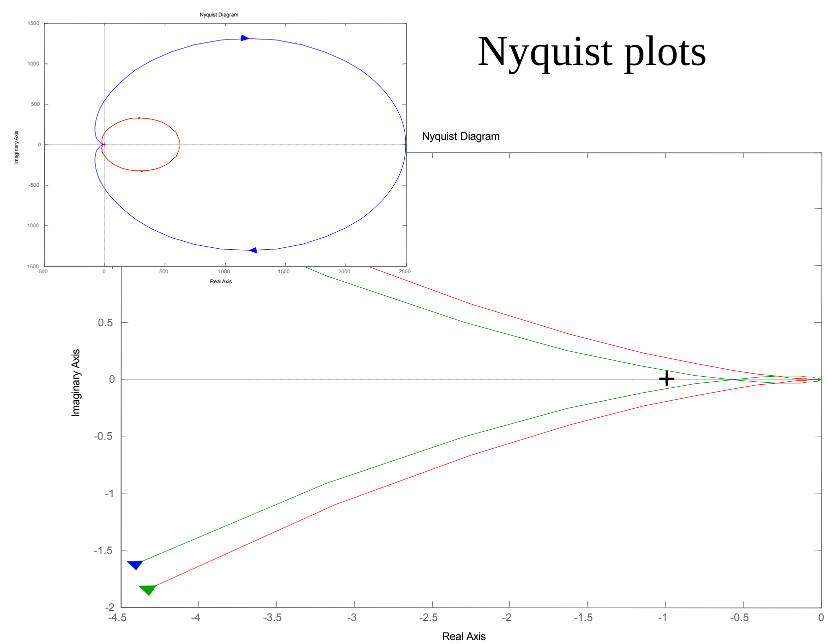
$$C(s) = \alpha \left(K_p + \frac{K_i}{s + 0.01} \right)$$

$$G(s) = \frac{10}{s + 10}$$

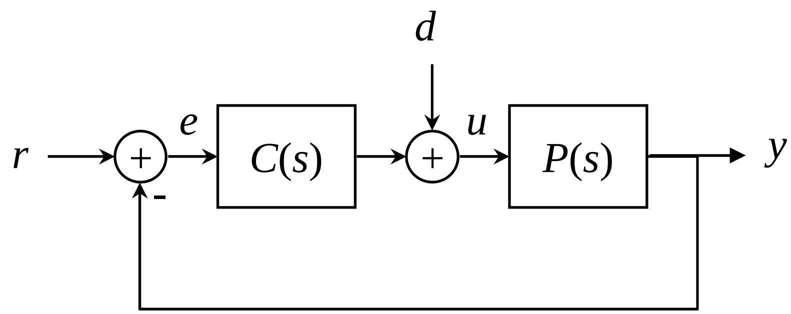
Approach: Increase phase margin

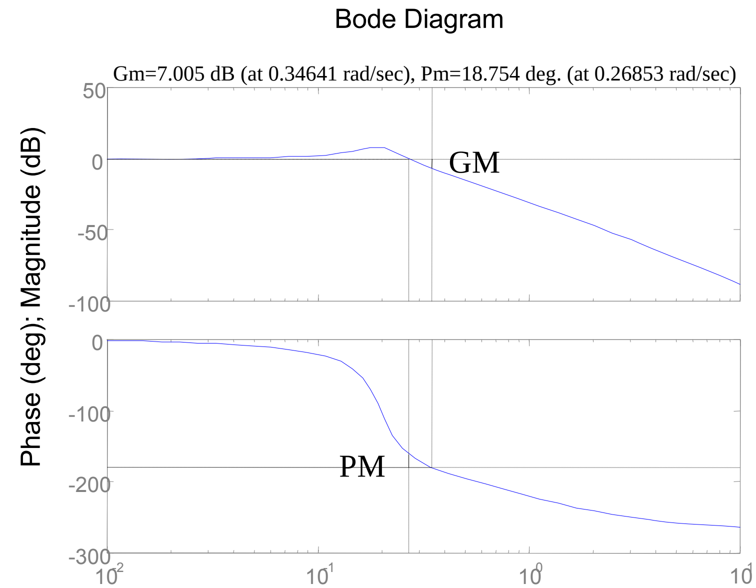
- Increase phase margin by reducing gain ⇒ can accommodate new sensor dynamics
- Tradeoff: lower gain at low frequencies ⇒ less bandwidth, larger steady state error



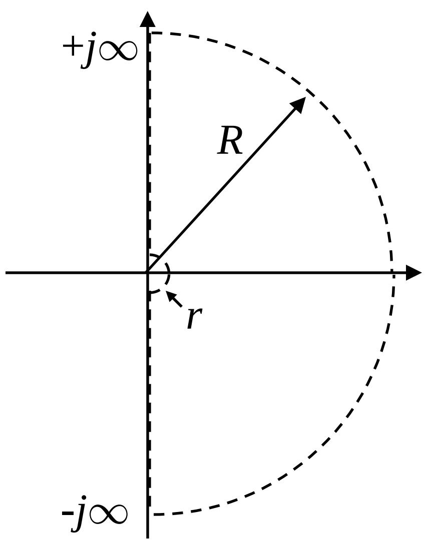


Summary: Loop Analysis of Feedback Systems





- Nyquist criteria for loop stability
- Gain, phase margin for robustness



Thm (Nyquist).

P # RHP poles of *L*(*s*)

N # CW encirclements

Z # RHP zeros

$$Z = N + P$$