

Nonlinear Control

Controllability and observability more challenging than for linear system

- Local concept
- Linearization may not give same answer

(e.g. parking a car:



introduce Lie algebra for formal analysis

- observability depends on control (doesn't decouple)

Control design.

1. Treat as nearly linear system, design control around each operating point
 ⇒ Gain scheduling

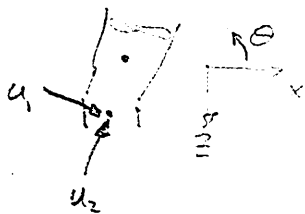
- Appropriate for slowly varying
 e.g. $\dot{x} = A(p)x + B(p)u$
 $\dot{p} = \dots$

• If linearization stable, nonlinear system is locally stable

- Prove w/ Lyapunov argument

2. Feedback linearization:

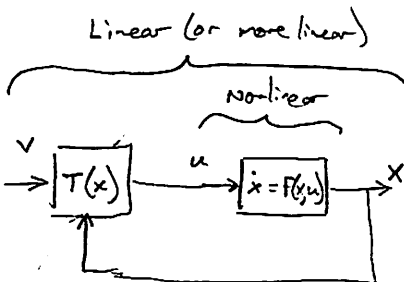
- Find ^{input and} state transformation that renders system linear



$$m\ddot{x} = -mg \cos\theta + u_1 \sin\theta + u_2 \cos\theta$$

$$m\ddot{z} = mg(1 - \sin\theta) + u_1 \cos\theta - u_2 \sin\theta$$

$$I\ddot{\theta} = r u_1 - I_f \Omega \dot{x} \cos\theta$$



Choose
$$\begin{bmatrix} v_1 \\ v_2 \end{bmatrix} = \begin{bmatrix} \sin\theta & \cos\theta \\ \cos\theta & -\sin\theta \end{bmatrix} \begin{bmatrix} u_1 \\ u_2 \end{bmatrix}$$

$$\Rightarrow \begin{bmatrix} u_1 \\ u_2 \end{bmatrix} = \begin{bmatrix} \sin\theta & \cos\theta \\ \cos\theta & -\sin\theta \end{bmatrix} \begin{bmatrix} v_1 \\ v_2 \end{bmatrix}$$

3. Lyapunov-based arguments

a) Backstepping: Recursive approach; reduce to low-order (simpler) problem & build up

E.g.

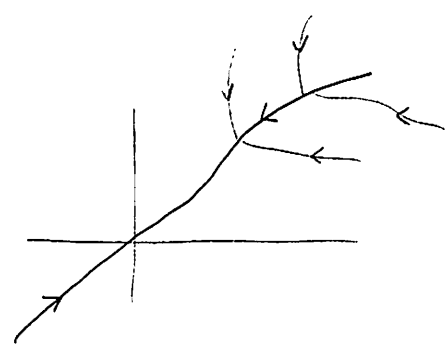
$$\dot{\eta} = F(\eta) + g(\eta) \xi$$

$$\dot{\xi} = u$$

- i) Design $\xi = \phi(\eta)$ to stabilize $\dot{\eta} = \dots$ subsystem
 - ii) Design u so that $\xi - \phi(\eta)$ is stable
- } Simultaneously stable

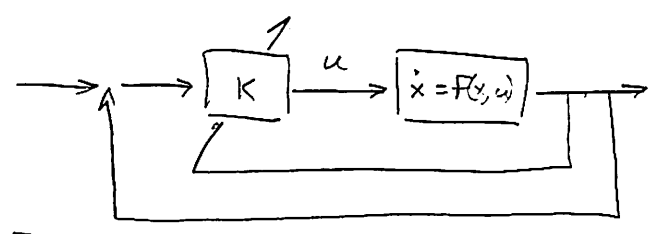
b) Sliding-mode: Robust

- Design to
- i) approach specified manifold in finite time (e.g. $\xi = \phi(\eta)$)



- ii) Converge to origin along manifold (e.g. if $\xi = \phi(\eta)$, then $\dot{\eta} = \dots$ stable)

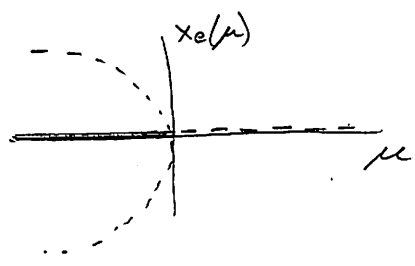
4. Adaptive control



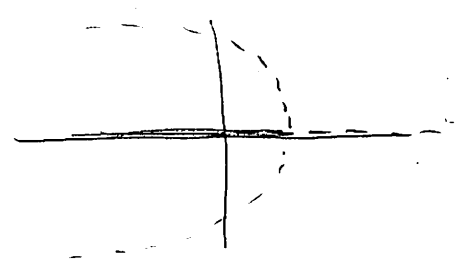
- E.g. model reference, update parameters of model
 - Can design control assuming plant known
 - Can estimate parameters (e.g. EKF) from output
- } combination not obviously stable...
- Relevant for linear but unknown system
- $$\dot{x} = A(p)x + B(p)u$$
- $$\dot{p} = \dots$$

5. Bifurcation control

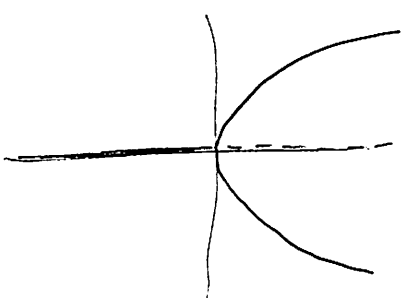
E.g. $\dot{x} = \mu x + x^3 + u$



subcritical pitchfork bifurcation



$u = -Kx$
increase stability but still subcritical



$u = -Kx^3$
supercritical

6. Optimization and Receding Horizon Control

$\dot{x} = f(x, u)$, and maybe constraints

$$J = \int_0^T L(x, u) dt + V(x(T))$$

choose $u = \text{argmin}(J)$

- Use Pontryagin to write conditions
- Solve 2P BVP
- Parameterize & discretize

RHC: Implement over ~~the~~

$t \in [t_0, t_0 + \delta]$, $\delta < T$,

and resolve over $t_1 = t_0 + \delta$ to $t_1 + T$

General, but need to worry about solving optimization in fixed known time.

Need conditions on V to guarantee stability (with Lyapunov)

Reachability & Controllability

(Isidori 1.8, 2.1-2.2)

Consider $\dot{x} = F(x) + g(x)u$ ^① (Affine)

$$y = h(x)$$

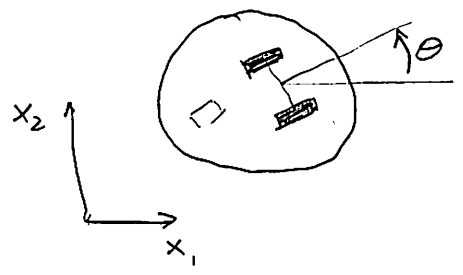
$$x \in M \subset \mathbb{R}^n, u \in K \subset \mathbb{R}^m$$

$$y \in \mathbb{R}^p$$

Definitions

- If $\exists u(t): [0, T] \rightarrow K$ Then $q = x(T) \in M$ satisfying ① with $x(0) = p$ is reachable from p in Time T
- The set of such q , $Q(p, T)$ is the Time-T reachable set (for $T=0$, $Q = p$)
- The system is controllable if $\forall p, q \in M, \exists T$ such that $q \in Q(p, T)$
- The system is small time locally controllable if p is an interior point of $Q(p, T)$

Example: "Planar drive vehicle" (roughly, unicycle, ...)



$$\text{with } u_1 = r_w (\tau_1 + \tau_2) \quad [\text{Forward force}]$$

$$u_2 = r_w (\tau_1 - \tau_2) \quad [\text{Torque}]$$

$$\text{So } \dot{x}_1 = u_1 \cos \theta$$

$$\dot{x}_2 = u_1 \sin \theta$$

$$\dot{\theta} = u_2$$

Note a non-holonomic constraint of no motion sideways.

E.g. linearize about $\theta = 0$:

$$\dot{x} = \underbrace{\begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix}}_A x + \underbrace{\begin{bmatrix} 1 & 0 \\ 0 & 0 \\ 0 & 1 \end{bmatrix}}_B u$$

Linear system is not controllable

$$\text{rank}([B \ AB \ A^2B]) = 2$$

(Aside:- linear system Then

$$x(t) = e^{At} x(0) + \underbrace{\int_0^t e^{A(t-\tau)} B u(\tau) d\tau}$$

$$= B\phi_0 + AB\phi_1 + A^2B\phi_2 + \dots$$

Controllable if $[B \ AB \ A^2B \ \dots]$ is full-rank

From Cayley-Hamilton, $A^n = \sum_{i=0}^{n-1} \alpha_i A^i$ for some α_i)

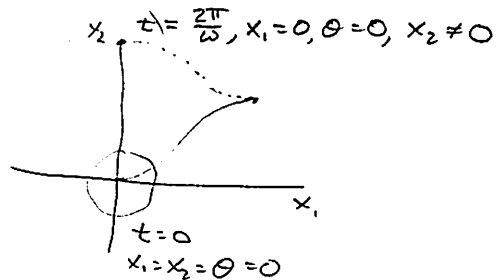
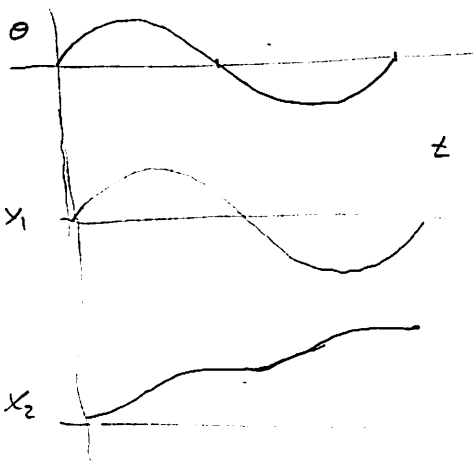
BUT nonlinear system is controllable:

E.g. $u_2 = \cos \omega t \Rightarrow \theta(t) = \frac{1}{\omega} \sin \omega t$ (with $\theta(0) = 0$)

$u_1 = \sin \omega t$

~~where $v_1 = u_1 - u_2(x_1 \sin \theta - x_2 \cos \theta)$ coordinate change~~

(Note, \exists nonlinear transformation where algebra is clean)



More

More general, for affine system

$$\dot{x} = F(x) + g_1(x)u_1 + g_2(x)u_2$$

Consider $u_1=1, u_2=0 \quad 0 \leq t < \epsilon$ & $F(x)=0$ for (Driftless)
 $u_1=0, u_2=1 \quad \epsilon \leq t < 2\epsilon$ simplicity
 $u_1=-1, u_2=0 \quad 2\epsilon \leq t < 3\epsilon$
 $u_1=0, u_2=-1, \quad 3\epsilon \leq t < 4\epsilon$

Then $x(\epsilon) = x_0 + \epsilon g_1(x_0) + \epsilon^2 \frac{1}{2} \frac{\partial g_1}{\partial x} g_1(x_0) + \text{h.o.t.}$

$$x(2\epsilon) = x_0 + \dots$$

$$+ \epsilon g_2(x_0 + \epsilon g_1(x_0) + \epsilon^2 \frac{1}{2} \frac{\partial g_1}{\partial x} g_1(x_0))$$

$$+ \epsilon^2 \frac{1}{2} \frac{\partial g_2}{\partial x} g_2(\dots) + \dots$$

$$\approx x(0) + \epsilon g_1(x_0) + \epsilon^2 \frac{1}{2} \frac{\partial g_1}{\partial x} g_1(x_0) + \epsilon g_2(x_0) + \epsilon^2 \frac{\partial g_2}{\partial x} g_1(x_0) + \epsilon^2 \frac{1}{2} \frac{\partial g_2}{\partial x} g_2(x_0)$$

$$\vdots$$

$$x(4\epsilon) = x_0 + \epsilon^2 \left[\frac{\partial g_2}{\partial x} g_1(x_0) - \frac{\partial g_1}{\partial x} g_2(x_0) \right]$$

Lie bracket $[g_1, g_2](x_0)$

→ Additional possible direction that cyclic control can move the system

$$= L_{g_1} g_2 - L_{g_2} g_1$$

derivative of g_2 along trajectory determined by g_1

E.g. for

$$\dot{x} = \underbrace{\begin{bmatrix} \cos x_3 \\ \sin x_3 \\ 0 \end{bmatrix}}_{g_1(x)} u_1 + \underbrace{\begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix}}_{g_2(x)} u_2$$

$$\text{Then } [g_1, g_2] = \frac{\partial g_2}{\partial x} g_1(x_0) - \frac{\partial g_1}{\partial x} g_2(x_0)$$

$$= 0 - \begin{bmatrix} 0 & 0 & -\sin x_3 \\ 0 & 0 & \cos x_3 \\ 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} = \begin{bmatrix} -\sin x_3 \\ \cos x_3 \\ 0 \end{bmatrix}$$

which is orthogonal to g_1, g_2

... The system is STLC if the set of vector fields

$$g_i, [g_i, g_j], [g_i, [g_i, g_k]], \dots \text{ spans the space}$$

⑦

With drift ($F(x) \neq 0$), Then

consider $\dot{x} = F(x)u_0 + g_1(x)u_1 + \dots$

where $u_0 = 1$

Then similarly take space $l_i, [l_i, l_i], [l_i, [l_i, l_k]]$ etc.
for $l_i \in \{F, g_i\}$

This doesn't quite give controllability, since u_0 is fixed

Note for linear system

$$\dot{x} = Ax + Bu = Ax + \sum b_i u_i$$

Then $[b_i, b_j] = 0$

and $[Ax, b_i] = -Ab_i$

$$[Ax, [Ax, b_i]] = A^2 b_i$$

Feedback linearization

When can we take a nonlinear system and transform it to a linear system? (NOT just locally?)

E.g. given $\dot{x} = f(x) + g(x)u$ $x \in \mathbb{R}^n$
 $y = h(x)$

Is there a transformation $z = T(x)$, $u = a(x) + b(x)v$ so that

$$\left. \begin{aligned} \dot{z} &= Az + Bv \\ y &= Cz \end{aligned} \right\} \text{Linear}$$

(If a NL system is feedback linearizable it is essentially linear!)

Note T must be diffeomorphism (invertible and smooth)
 - In practice only locally diffeomorphic

Define relative degree: how many times differentiate y before u shows up explicitly?

relative degree r if $L_g L_f^k h(x) = 0 \quad \forall x$ in nbhd of x_0
 $L_g L_f^{r-1} h(x) \neq 0 \quad \& \quad k < r-1$

(For linear system, difference between degree of numerator & denominator)

$$H(s) = C(sI - A)^{-1}B = \frac{b_{n-r}s^{n-r} + \dots + b_0}{s^n + a_{n-1}s^{n-1} + \dots + a_0} \quad \text{and} \quad L_g L_f^k h = CA^k Bx$$

SISO

Suppose relative degree is n (NO zero dynamics)

Then $y = h(x)$ ↖ can't have $r > n$

$$y^{(1)} = L_f h(x)$$

$$y^{(n-1)} = L_f^{n-1} h(x)$$

$$y^{(n)} = L_f^n h(x) + L_g L_f^{n-1} h(x)u$$

Then $z = T(x) = \begin{bmatrix} z_1 \\ z_2 \\ \vdots \\ z_r \end{bmatrix} = \begin{bmatrix} y \\ \dot{y} \\ \vdots \\ y^{(r-1)} \end{bmatrix} = \begin{bmatrix} h(x) \\ L_F h(x) \\ \vdots \\ L_F^{r-1} h(x) \end{bmatrix}$

puts system in "normal form" ...

$$\dot{z}_1 = z_2$$

$$\dot{z}_2 = z_3$$

⋮

$$\dot{z}_r = \underbrace{L_F^r h(x) + L_g L_F^{r-1} h(x) u}_v$$

$$\& u = \frac{1}{L_g L_F^{r-1} h(x)} (-L_F^r h(x) + v)$$

or

$$\dot{z} = \begin{bmatrix} 0 & 1 & 0 & \dots \\ 0 & 0 & 1 & \dots \\ & & & \ddots \\ & & & 0 \end{bmatrix} z + \begin{bmatrix} 0 \\ \vdots \\ 0 \\ 1 \end{bmatrix} u$$

[& e.g. $v = -Kz$ (state feedback) can arbitrarily place poles of closed-loop system]

$$A - BK = \begin{bmatrix} 0 & 1 & \dots \\ & & \ddots \\ -k_1 & -k_2 & \dots & -k_n \end{bmatrix}, \lambda(A - BK) = \det(\lambda I - (A - BK)) = \dots$$

IF $r < n$ need to:

- 1) Construct Transformation for z_{r+1} to z_n (and show that exists)
- 2) Understand stability of the "zero dynamics"

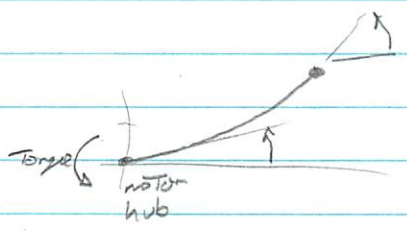
In general, if can construct some output $y = h(x)$ with relative degree n , Then $\dot{x} = F(x) + g(x)u$ is feedback linearizable.

(Can write as conditions involving $[g, \cdot]$, $[F, g]$, $[F, [F, g]]$, ... need each of these involutive and constant dimensional)

Example:

Euler equations (rigid body rotation) with two inputs (e.g. momentum wheels)

$$\begin{aligned} \dot{\omega}_1 &= A_1 \omega_2 \omega_3 + u_1 \\ \dot{\omega}_2 &= A_2 \omega_1 \omega_3 + u_2 \\ \dot{\omega}_3 &= A_3 \omega_2 \omega_1 \end{aligned}$$



Single-link manipulator

$$\begin{aligned} I \ddot{q}_1 + M_g L \sin q_1 + k(q_1 - q_2) &= 0 \\ I \ddot{q}_2 - k(q_1 - q_2) &= u \end{aligned}$$

or $F(x) = \begin{bmatrix} x_2 \\ -a \sin x_1 - b(x_1 - x_3) \\ x_4 \\ c(x_1 - x_3) \end{bmatrix}, \quad g = \begin{bmatrix} 0 \\ 0 \\ 0 \\ d \end{bmatrix}$ for some constants $a, b, c, d > 0$

IF $y = x_1$, choose

$$\begin{aligned} z_1 &= x_1 \quad (= h(x)) \\ z_2 &= L_f h(x) = x_2 \\ z_3 &= L_f^2 h(x) = -a \sin x_1 - b(x_1 - x_3) \\ z_4 &= L_f^3 h(x) = a x_2 \cos x_1 - b(x_2 - x_4) \end{aligned}$$

$$\Rightarrow \dot{z}_1 = z_2, \quad \dot{z}_2 = z_3, \quad \dot{z}_3 = z_4, \quad \dot{z}_4 = - (a \cos z_1 + b + c) z_3 + a(z_2^2 - c) \sin z_1 + b d u = v$$

This transformation is valid globally since $z = T(x)$ is globally diffeomorphic (except $x_1 = 0, \pm \pi/2$)