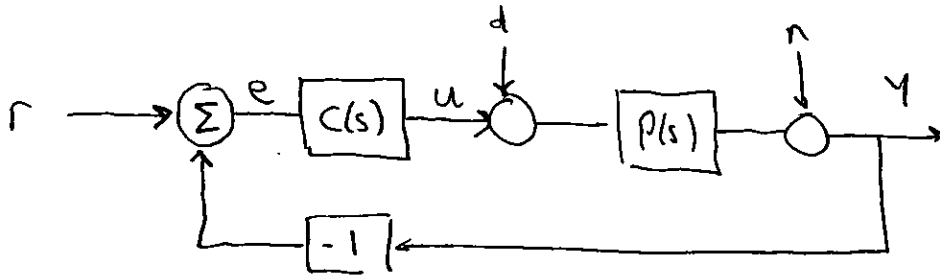


# Lecture 6-2: Frequency Response

①

Linear (or linearized) control system:



Controller design goals:

- Keep  $e(t)$  "small" in presence of disturbances ( $d$ ), sensor noise ( $n$ ) and changes in reference ( $r$ )

- Time domain: given  $r(t)$ ,  $d(t)$  or  $n(t)$ , would like  $\|e\| < \gamma \|d\|$  (or  $n$  or  $r$ )

↑ "size" of error signal  
↑ "gain"  
↑ "size of disturbance"

- Frequency domain:  $|H_{ed}(j\omega)|$  small for all  $\omega$

$$\Rightarrow d = A \sin(\omega t) \rightarrow e = A |H_{ed}(j\omega)| \sin(\omega t + \phi(\omega))$$

◦ For control analysis (and design), focus on four, *the* key transfer functions

$$\text{Keep small } \left\{ \begin{array}{l} H_{er} = \frac{1}{1+PC} \\ H_{ed} = \frac{P}{1+PC} \end{array} \right. \quad \left. \begin{array}{l} H_{ru} = \frac{C}{1+PC} \\ \underbrace{H_{yr} = H_{du}}_{\text{Keep near 1}} = \frac{PC}{1+PC} \end{array} \right\} \text{ "Gang of Four"}$$

Example: PI cruise controller

System:

$$m \frac{dv}{dt} = a_n u T(a_n v) - m g C_r \operatorname{sgn}(v) - \frac{1}{2} \rho C_d A v^2 - m g \sin \Theta$$

$y = v \leftarrow$  output.

Linearize around  $v_e = 20 \text{ m/sec}$  ( $\approx 40 \text{ mph}$ ),  $\Theta = 0$ ,  $n = 4$

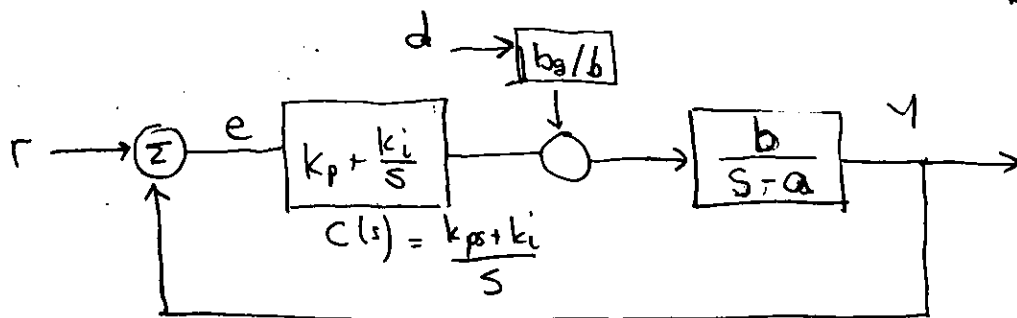
Let  $e = v - v_e$ ,  $\tilde{u} = u - u_e$ ,  $d = \Theta - 0$

$$\dot{e} = a e + b \tilde{u} + b_g d \quad P(s)$$

$$\left. \begin{array}{l} a = -0.01 \\ b = 1.32 \approx 1 \\ b_g = 9.8 \approx 10 \end{array} \right\} \begin{array}{l} \text{Ex} \\ \text{S.11} \end{array}$$

Controller:  $\tilde{u} = k_p e + k_i \int_0^+ e$

$$\left. \begin{array}{l} k_p = 0.5 \\ k_i = 0.1 \end{array} \right\} \begin{array}{l} \text{Later} \\ \text{(ch 10)} \end{array}$$



Transfer functions:

$$H_{yr} = \frac{PC}{1+PC} = \frac{b(k_p s + k_i)}{s^2 + (bk_p - a)s + bk_i}$$

Zeros:  $0, -k_i/k_p$

Poles:  $(a - bk_p)/2$

$$\pm \sqrt{(a - bk_p)^2/4 - bk_i}$$

$$H_{ed} = \frac{(b_g/b)P}{1+PC} = \frac{b_g s}{s^2 + (bk_p - a)s + bk_i}$$

(3a)

## Reference tracking

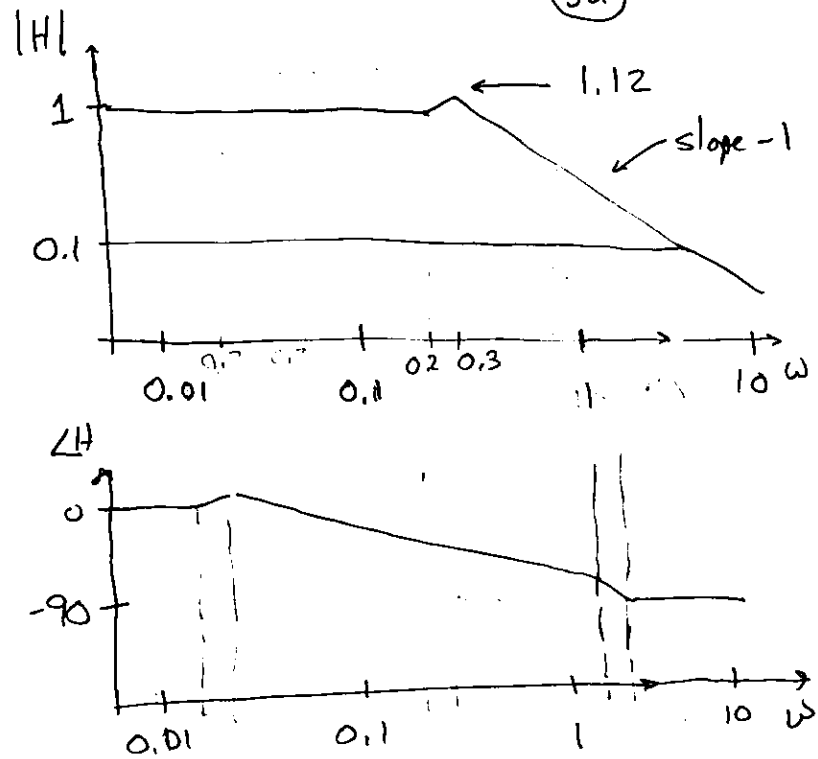
$$H_{yr} = \frac{b(s k_p + k_i)}{s^2 + (b k_p - a)s + b k_i}$$

$$\text{Poles: } s^2 + 2\zeta\omega_n s + \omega_n^2$$

$$\omega_n^2 = 0.1 \Rightarrow \omega_n \approx 0.32$$

$$2\zeta\omega_n \approx 0.5 \Rightarrow \zeta \approx 0.78$$

$$\text{Zeros: } s = -\frac{k_i}{k_p} = -0.2$$



Value at peak:

$$|H_{yr}(i\omega_n)| = \left| \frac{b(i\omega_n k_p + k_i)}{2\zeta\omega_n^2} \right| = \frac{b\sqrt{\omega_n^2 k_p^2 + k_i^2}}{2\zeta\omega_n^2} \approx 1.12$$

Implications

1. Get perfect tracking for constant inputs ( $\omega = 0$ )
2. Oscillating reference at  $\sim 0.32$  rad/sec ( $\sim 20$  secs/cycle) gives slight error (12%)
3. Higher frequencies can't be tracked; get large errors

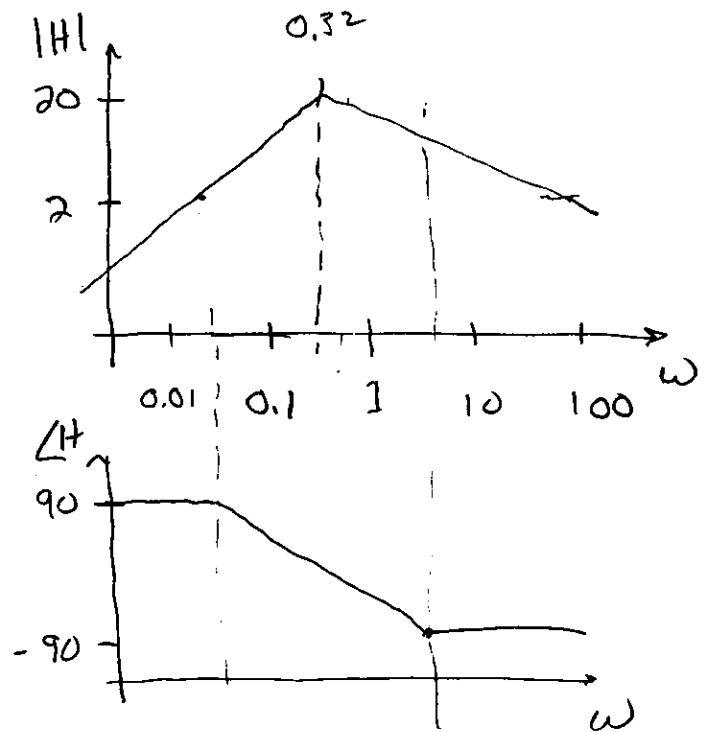
## Disturbance rejection

$$H_{ed} = \frac{b_g s}{s^2 + (b k_p - a) s + b k_i}$$

Poles:  $s^2 + 2\zeta\omega_n s + \omega_n^2$

$$\omega_n^2 = 0.1 \Rightarrow \omega_n \approx 0.32$$

$$2\zeta\omega_n = 0.5 \Rightarrow \zeta \approx 0.75$$



Value at peak:

$$|H_{ed}(i\omega_n)| = \frac{b_g \omega_n}{2\zeta\omega_n^2} = \frac{b_g}{2\zeta\omega_n} = \frac{10}{1.5 \times 0.3} \approx 20$$

Implications

1. Constant disturbance  $\Rightarrow$  zero error
2. Hills at 0.32 rad/sec ( $\approx$  20 secs/cycle)  
 $\Rightarrow$  amplification!
3. How do we design better disturbance rejection?

A: Choose  $2\zeta\omega_n$  larger  $\Rightarrow (b k_p - a) \sqrt{b k_i}$  larger  
 $\circ$  increase  $k_p$  or  $k_i$  (or both)

BUT Will see next week there are limits...

(skip)

Reference error

$$H_{er} = \frac{s(s-a)}{s^2 + (bk_p - a)s + bk_i}$$

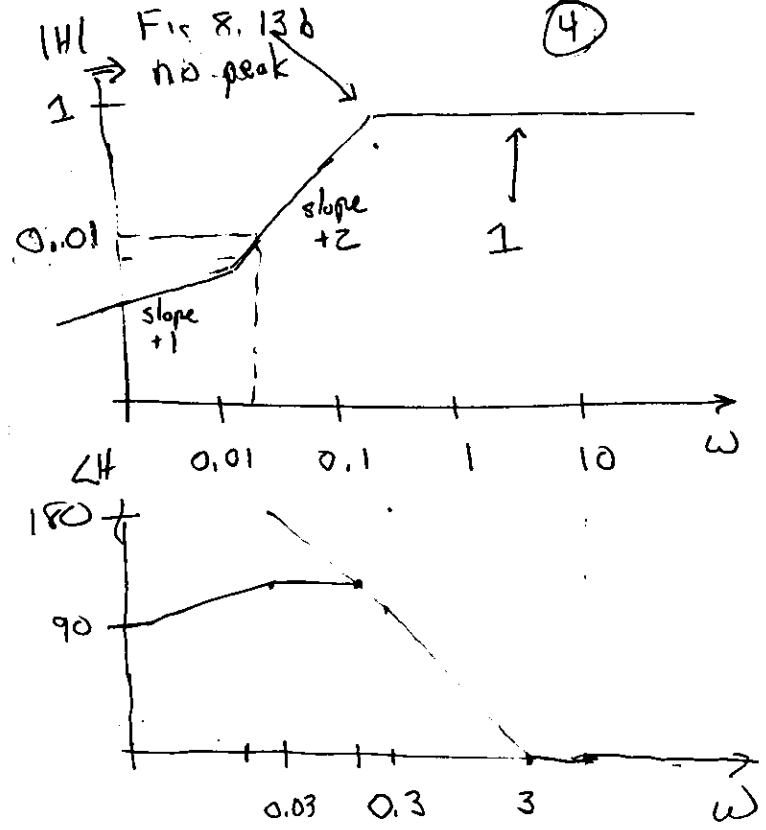
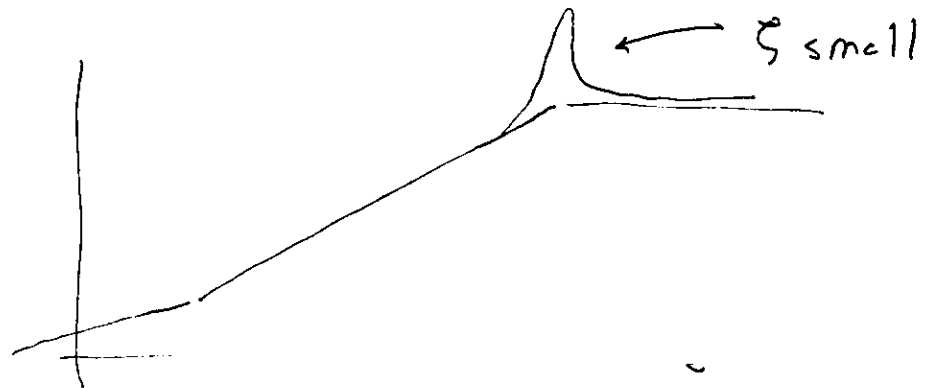
Poles:  $s^2 + 2\zeta\omega_n s + \omega_n^2$

$$\omega_n^2 = 0.1 \Rightarrow \omega_n \approx 0.32$$

$$2\zeta\omega_n \approx 0.5 \Rightarrow \zeta \approx 0.78$$

Implications

- Constant reference  $\Rightarrow$  zero error (integral action)
- High frequency reference ( $2\pi$  rad/sec = 1 Hz)
- What if you want more performance?  
 Ai move  $\omega_n$  higher  $\Rightarrow$  increase  $k_i$   
 But increasing  $\omega_n$  decreases  $\zeta \Rightarrow$  get resonance



Homework: similar analysis with additional dynamics for the engine (and slightly diff parameters)

Big picture

$$\left. \begin{array}{l} \dot{x} = f(x, u, d) \\ y = h(x) + n \end{array} \right\} \text{Trajectory generation}$$

$$\left. \begin{array}{l} \dot{x}_d = f(x_d, u_d, 0) \\ r = h(x_d, 0) \end{array} \right\}$$

## Error dynamics

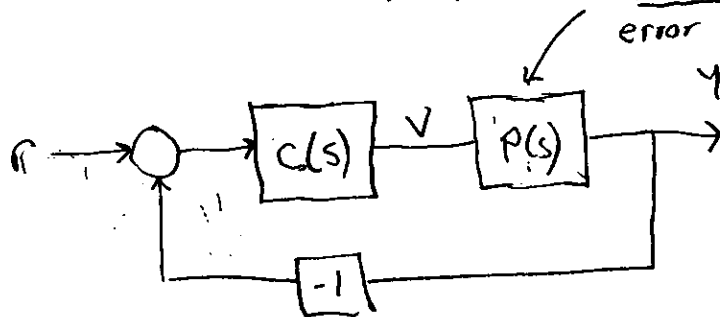
$$\begin{aligned} e &= x - x_d \\ v &= u - u_d \\ \dot{e} &= f(x, u, d) - f(x_d, u_d, 0) \\ &= f(x_d + e, u_d + v, d) - f(x_d, u_d, 0) \\ &\approx A(x_d)e + B(x_d)v + F(x_d)d \end{aligned}$$

$$A(x_d) = \frac{\partial f}{\partial x} \Big|_{(x_d, u_d)} \quad B(x_d) = \frac{\partial f}{\partial u} \Big|_{(x_d, u_d)} \text{ etc}$$

linearized error dynamics

## Controller design

$$v = C(s)(r - y)$$



Overall controller:  $u = u_d + v$

What's next

1. Need to make sure closed loop system is stable:

$$H_{er} = \frac{1}{1 + PC} \Rightarrow \text{zeros of } 1 + PC \text{ in LHP}$$

2. Need to design  $C(s)$  to achieve performance specs (trajectory tracking, disturbance/noise rejection)

3. Study robustness of closed loop: what if  $P(s) \rightarrow \tilde{P}(s)$