



CDS 101: Lecture 9.2 PID and Root Locus



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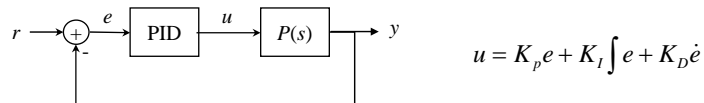
Goals:

- Define PID controllers and describe how to use them
- Describe root locus diagram and show how to use it to choose loop gain

Reading:

- Astrom, Sec 6.1-6.4, 6.6
- *Optional*: PPH, Sec 13
- *Advanced*: Lewis, Chapter 12 + Sec 13.1

Overview: PID control



Intuition

- Proportional term: provides inputs that correct for “current” errors
- Integral term: insures *steady state* error goes to zero
- Derivative term: provides “anticipation” of upcoming changes

A bit of history on “three term control”

- First appeared in 1922 paper by Minorsky: “Directional stability of automatically steered bodies” under the name “three term control”
- Also realized that “small deviations” (linearization) could be used to understand the (nonlinear) system dynamics under control

Utility of PID

- PID control is most common feedback structure in engineering systems
- For many systems, only need PI or PD (special case)
- Many tools for tuning PID loops and designing gains (see reading)

Frequency domain compensation with PID

$$C(s) = K_p + K_I \cdot \frac{1}{s} + K_D s$$

$$= k \left(1 + \frac{1}{T_I s} + T_D s \right)$$

$$= \frac{k T_D}{T_I} \frac{(s + 1/T_I)(s + 1/T_D)}{s}$$

Bode Diagrams

Transfer function for PID controller

$$u = K_p e + K_I \int e + K_D \dot{e}$$

$$H_{ue}(s) = K_p + K_I \cdot \frac{1}{s} + K_D s$$

- Roughly equivalent to a PI controller with lead compensation
- Idea: gives high gain at low frequency plus phase lead at high frequency
- Place below desired crossover freq

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Tools for Designing PID controllers

$$C(s) = K \left(1 + \frac{1}{T_I s} + T_D s \right)$$

Zeigler-Nichols tuning

- Design PID gains based on step response
- Works OK for many plants (but underdamped)
- Good way to get a first cut controller
- Frequency domain version also exists

Caution: PID amplifies high frequency noise

- Sol'n: pole at high frequency

Caution: Integrator windup

- Prolonged error causes large integrated error
- Effect: large undershoot (to reset integrator)
- Sol'n: move pole at zero to very small value
- Fancier sol'n: anti-windup compensation

Step response

$$K = 1.2 / a \quad T_I = 2 * L \quad T_D = L / 2$$

Bode Diagrams

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PID vs lead/lag compensation

PID Control

$$C(s) = K_p + K_I \cdot \frac{1}{s} + K_D s$$

Bode Diagram

Pros: easy to design, implement
Cons: low freq lag, high freq gain

Lead/Lag Compensation

$$C(s) = K \frac{s + a_{lag}}{s + b_{lag}} \cdot \frac{s + a_{lead}}{s + b_{lead}}$$

Bode Diagram

Pros: low freq phase, high freq rolloff
Cons: more complicated (slightly)

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Example: PID cruise control

$$P(s) = \frac{1/m}{s + b/m} \cdot \frac{r}{s + a}$$

Ziegler-Nichols design for cruise controller

- Plot step response, extract L and a , compute gains

Bode Diagrams

Step Response

$$C(s) = K \left(1 + \frac{1}{T_I s} + T_D s \right)$$

$K = 1.2/a \quad T_I = 2 * L \quad T_D = L/2$

• Result: *sluggish* \Rightarrow increase loop gain

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Pole Zero Diagrams and Root Locus Plots

Pole zero diagram verifies stability

- Roots of $1 + PC$ give closed loop poles
- Can *trace* the poles as a parameter is changed:

$$C(s) = K \left(1 + \frac{1}{T_I s} + T_D s \right)$$

alpha points to T_I

Original pole location ($\alpha = 0$)

Pole goes unstable for some α

Pole goes to ∞

Poles merge and split

Pole goes to terminal value

Root locus = locus of roots as parameter value is changed

- Can plot pole location versus *any* parameter; just repeatedly solve for roots
- Common choice in control is to vary the loop gain (K)

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One Parameter Root Locus

Basic idea: convert to "standard problem": $a(s) + \alpha b(s) = 0$

- Look at location of roots as α is varied over *positive real* numbers
- If "phase" of $a(s)/b(s) = 180^\circ$, we can always choose a real α to solve eqn
- Can compute the phase from the pole/zero diagram

$s_0 - (-p_1) = s_0 + p_1$

$\phi_1 =$ phase contribution from s_0 to $-p_1$

$\psi_1 =$ phase contribution from s_0 to $-z_1$

$$G(s) = \frac{a(s)}{b(s)} = k \frac{(s + z_1)(s + z_2) \cdots (s + z_m)}{(s + p_1)(s + p_2) \cdots (s + p_n)}$$

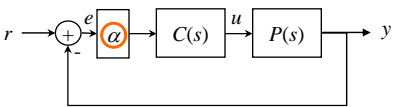
$$\angle G(s_0) = \angle(s_0 + z_1) + \cdots + \angle(s_0 + z_m) - \angle(s_0 + p_1) - \cdots - \angle(s_0 + p_n)$$

Trace out positions in plane where phase = 180°

- At each of these points, there exists gain α to satisfy $a(s) + \alpha b(s) = 0$
- All such points are on *root locus*

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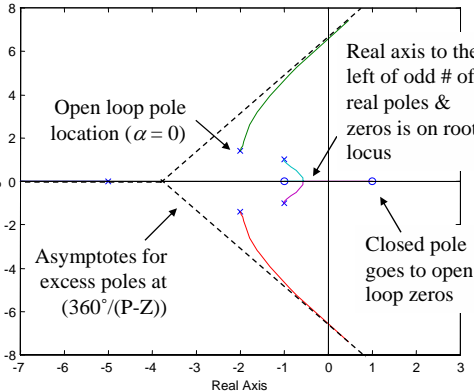
Root Locus for Loop Gain



$$1 + \alpha \frac{n(s)}{d(s)} \rightarrow d(s) + \alpha n(s) = 0$$

Loop gain as root locus parameter

- Common choice for control design
- Special properties for loop gain
 - Roots go from poles of PC to zeros of PC
 - Excess poles go to infinity
 - Can compute asymptotes, break points, etc
- Very useful tool for control design
- MATLAB: rlocus



Additional comments

- Although loop gain is the most common parameter, *don't forget* that you can plot roots versus *any* parameter
- Need to link root location to performance...

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Second Order System Response

Second order system response

- Spring mass dynamics, written in canonical form

$$H(s) = \frac{\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2} = \frac{\omega_n^2}{(s + \zeta\omega_n + j\omega_d)(s + \zeta\omega_n - j\omega_d)} \quad \omega_d = \omega_n \sqrt{1 - \zeta^2}$$

• Performance specifications

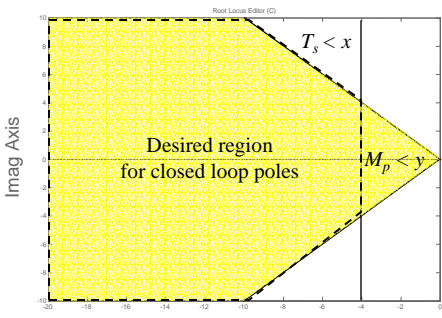
$$T_r \approx 1.8 / \omega_n \quad M_p \approx e^{-\pi\zeta / \sqrt{1 - \zeta^2}}$$

$$T_s \approx 3.9 / \zeta\omega_n \quad e_{ss} = 0$$

ζ	M_p	Slope
0.707	4%	-1
0.5	16%	-1.7
0.25	44%	-3.9

Guidelines for pole placement

- Damping ratio gives Re/Im ratio
- Setting time determined by $-\text{Re}(\lambda)$



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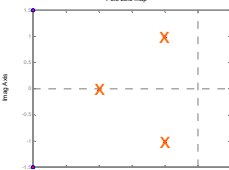
Effect of pole location on performance

Idea: look at “dominant poles”

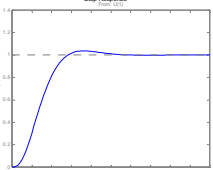
- Poles nearest the imaginary axis (nearest to instability)
- Analyze using analogy to second order system

PZmap complements information on Bode/Nyquist plots

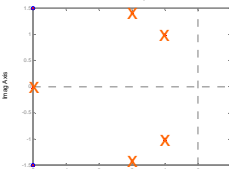
- Similar to gain and phase calculations
- Shows performance in terms of the *closed* loop poles
- Particularly useful for choosing system gain
- Also useful for deciding where to put controller poles and zeros (with practice [and SISOTool])



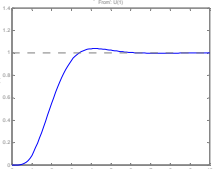
Pole-zero map



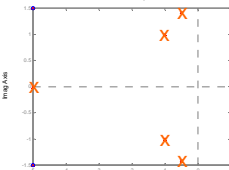
Step Response



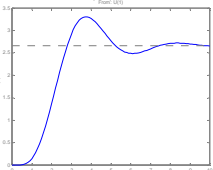
Pole-zero map



Step Response



Pole-zero map



Step Response

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Example: PID cruise control

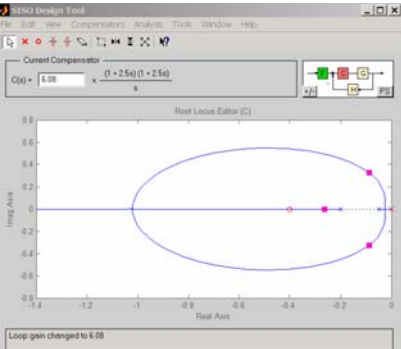
Start with PID control design:

$$P(s) = \frac{1/m}{s + b/m} \cdot \frac{r}{s + a}$$

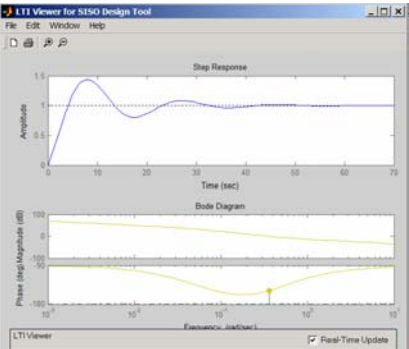
$$C(s) = K \left(1 + \frac{1}{T_I s} + T_D s \right)$$

Modify gain to improve performance

- Use MATLAB sisotool
- Adjust loop gain (K) to reduce overshoot and decrease settling time
 - $\zeta \approx 1 \Rightarrow$ less than 5% overshoot
 - $\text{Re}(p) < -0.5 \Rightarrow T_s$ less than 2 sec




Root Locus Editor (C)

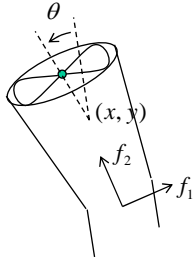


LTI Viewer for SISOTool

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Example: Ducted fan lateral position control

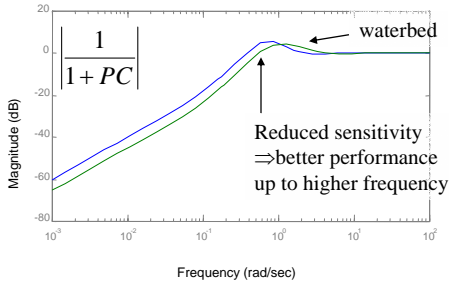




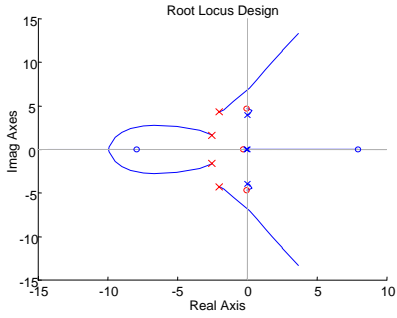
$$P(s) = \frac{(s^2 - mgl)}{s^2(Js^2 + ds + mgl)}$$

Lateral control (x)

- Right half plane zero makes design very tricky using y as output



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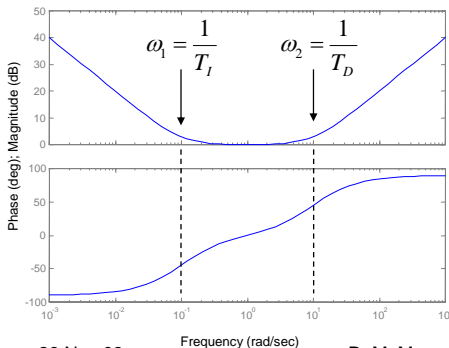
Summary: PID and Root Locus

PID control design

- Very common (and classical) control technique
- Good tools for choosing gains

$$u = K_p e + K_I \int e + K_D \dot{e}$$

Bode Diagrams



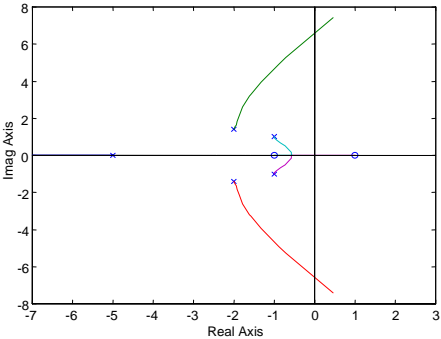
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Root locus

- Show closed loop poles as function of a free parameter

Performance limits

- RHP poles and zeros place limits on achievable performance
- Waterbed effect



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