

Trajectories to the Moons (incl. a trajectory for an Enceladus orbiter)

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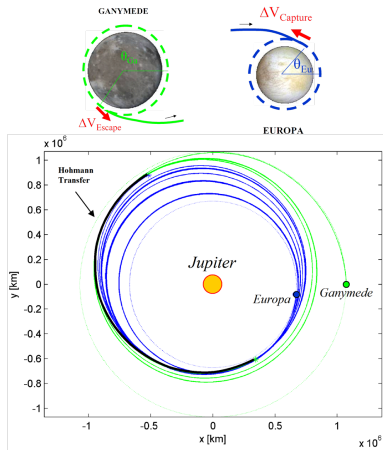
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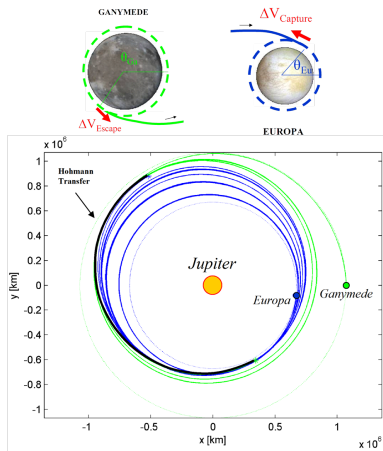
Problem Definition and Motivation

- ▶ Trajectories for the exploration of planetary moons (e.g.: Galileo, Cassini)
- ▶ Motivation: Orbiters for Missions to the Jupiter Moons; Missions to the Saturn Moons
- ▶ Aim: Achieve a low $\Delta V_{capture}$ and or ΔV_{escape} at a moon and a low Time of Flight (ToF)



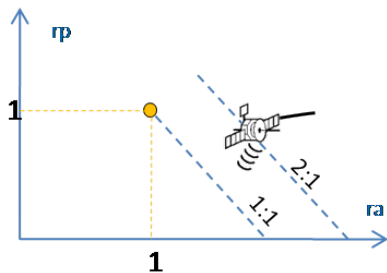
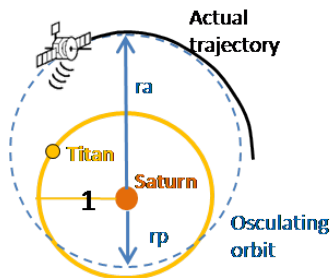
Problem Definition and Motivation

- ▶ Trajectories for the exploration of planetary moons (e.g.: Galileo, Cassini)
- ▶ Deep space maneuvers ΔV_{DSM}
- ▶ Flybys at the same moon and/or at different moons
- ▶ Pareto front $\min(ToF, \Delta V_{TOT})$, where
$$\Delta V_{TOT} = \Delta V_{capture/escape} + \Delta V_{DSM}$$
- ▶ Models : patched 2-body problems or patched 3-body problems



r_a, r_p, T

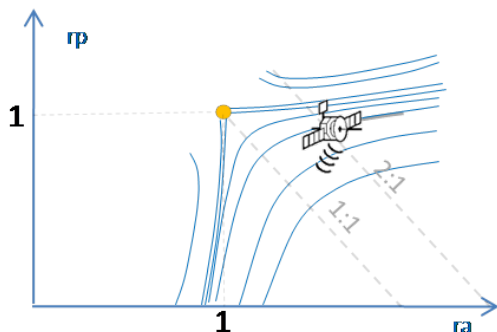
- ▶ Assume the s/c is orbiting the major body (Saturn, Jupiter).
- ▶ We represent each point of its trajectory in coordinates with the **osculating apocenter and pericenter**.



ra, rp, T

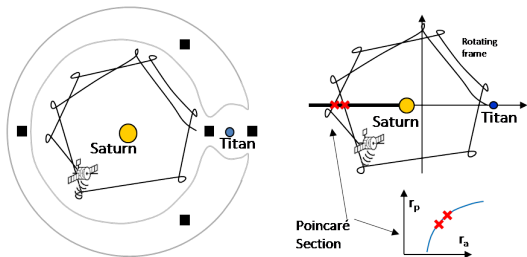
The s/c trajectory is not a keplerian orbit: the perturbation from the nearest and most massive moon changes the osculating pericenter and apocenter. Yet far from the moon, before and after a flyby, the **Tisserand parameter** remains approximately constant. Why? What is the Tisserand parameter?

$$T = \frac{2}{r_a + r_p} + 2\sqrt{\frac{2r_a r_p}{r_a + r_p}}$$



T-P graph and the CR3BP

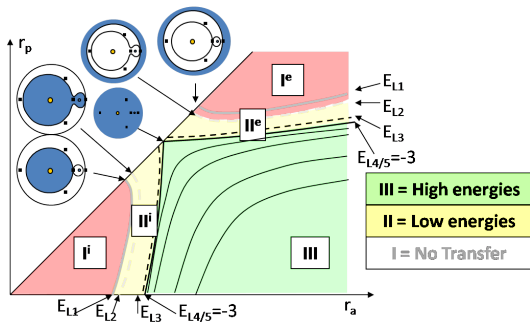
In the circular restricted three-body problem (CR3BP) model, $T \cong J = -E$ when the third body is far from the minor body. If we put a Poincaré section on the negative x axis of the rot. frame, the osculating r_a, r_p at the crossing will stay on the same Tisserand level set. **T-P (Tisserand-Poincaré) graph**



T-P graph and the CR3BP

We can find Energy regions in the T-P graph. In particular, High Energies and Low Energies.

High Energies \rightarrow High $\Delta V_{capture}$; Low Energies \rightarrow Low $\Delta V_{capture}$



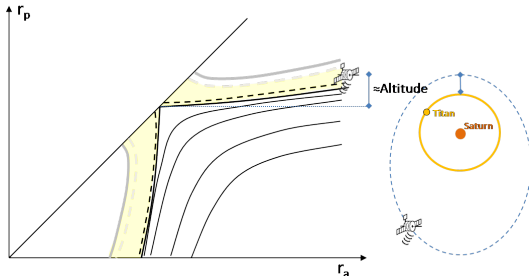
Paradox of the Low Energy Transfers

$\Delta V_{\text{esc/capt}}$ depends *mostly* on $J = -E$

Flybys at the target moon do not change $J = -E$

Flybys at the target moon
(with no ΔV_{DSM}) cannot
decrease mission costs

In the Low Energy domain, at high r_a (after Saturn orbit insertion), $r_p > 1$. (The closest approach at Titan @ tens of thousands kilometers).
PARADOX solution: (high-altitude) flybys brings the spacecraft closer to the Moon, leading to a low-altitude, Low-Energy orbit insertion.

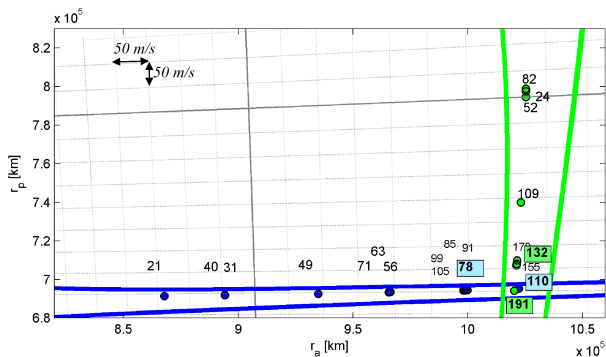


Low Energy Transfers

- ▶ Initial altitude too high \rightarrow quasiballistic transfers require several high-altitude flybys to reach the final orbit (Smart1, Multimoon Orbiter, Keplerian Map) \rightarrow long ToF.
- ▶ Low orbit insertion cost \rightarrow low ΔV_{TOT} (even ballistic transfers to/from Halo orbits).
- ▶ ToF can be reduced introducing ΔV_{DSM} to jump between “good” resonances (a 6:5 better than a 17:15). Work in Progress.

Ganymede-Europa

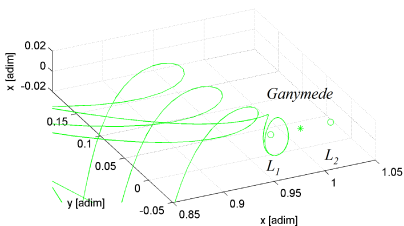
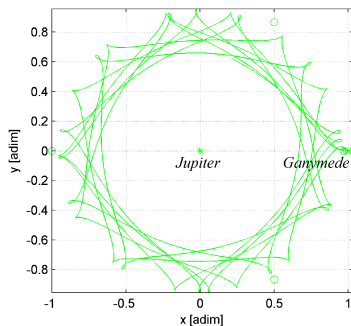
Example: From L1 - Halo orbit around Ganymede, to a L2 - Halo orbit around Europa.



$\Delta V_{tot} = \Delta V_{DSM} \approx 50 \text{ m/s}$, 10 months (or 8 months and 100 m/s).
Hohmann transfer $> 2 \text{ km/s}$!

Ganymede-Europa

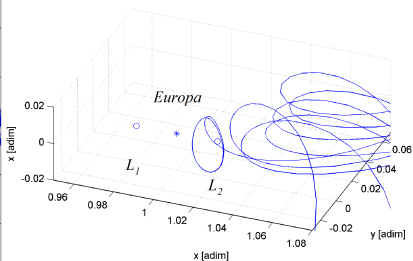
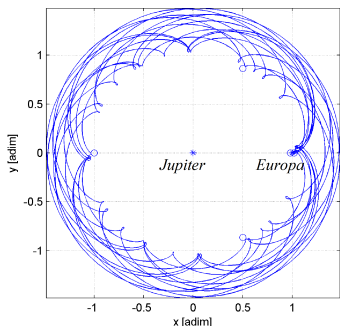
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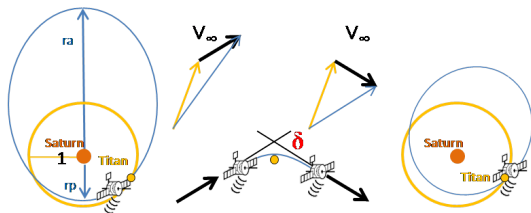


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T-P graph and the patched 2BP (High Energy)

- ▶ Low-energy transfers can provide large ΔV savings for the orbit insertion.
- ▶ Other part of the missions can have flybys at the moon without orbit insertion (Cassini, Galileo).
- ▶ Then it is more efficient to navigate the spacecraft in the High-Energy regime, where low-altitude flybys provide a larger controllability and shorter ToF with no additional ΔV .
- ▶ Design is also simpler because in this domain we can use *linked conics*, and the solutions to the 2 Body Problem (2BP).
- ▶ The special case: Enceladus Orbiter. Very small moons: Rhea, next largest moon, has 2% of Titan's mass. Enceladus radius is only 250 km, $GM = 7$ and its orbit is at 4 Saturn Radii.

T-P graph and the patched 2BP (High Energy)



In the linked conic model, trajectories are made of conics linked by flybys or maneuvers. Flybys only occur if $rp < 1$, $ra > 1$, and change the relative velocity v_∞ by

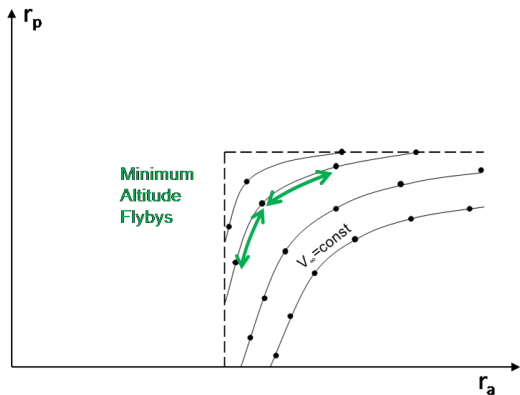
$$\delta = \arcsin \left(\frac{\mu_M}{\mu_M + v_\infty^2 (r_M + h)} \right)$$

Before and after a flyby: $|v_\infty| = \text{const}$. In fact it can be proved that:

$$T = 3 - v_\infty^2$$

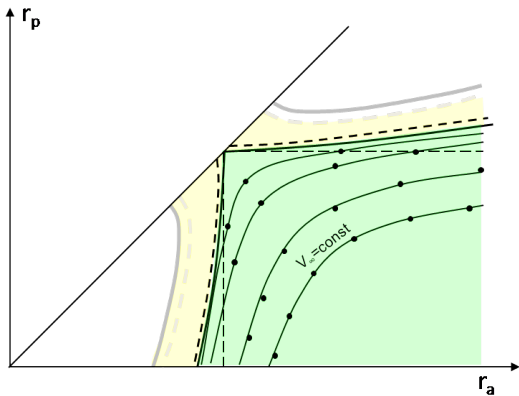
T-P graph and the patched 2BP (High Energy)

The *Tisserand graph* is a graphical method used in orbital mechanics to study flyby trajectories in the linked conic model. Here we introduce a $ra - rp$ representation.



T-P graph and the patched 2BP (High Energy)

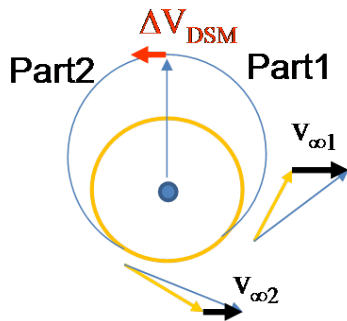
The *Tisserand graph* is a graphical method used in orbital mechanics to study flyby trajectories in the linked conic model. Here we introduce a $r_a - r_p$ representation.



The Tisserand graph is the restriction of the T-P graph to the $r_a > 1, r_p < 1$ (High Energy) domain!

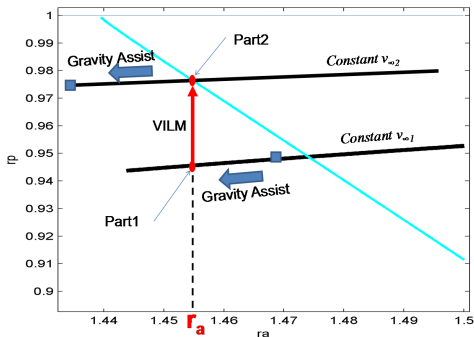
High Energy Transfers

- ▶ Reducing the ToF for the Enceladus Orbiter: leveraging the Energies with flybys and ΔV_{DSM} to jump between good resonances.
- ▶ Representation on the T-P (Tisserand) graph: ΔV_{DSM} at ra (rp) are vertical (*horizontal*) shift.
- ▶ Solving the phasing using Kepler's equation yields to $f(v_{\infty 1}, v_{\infty 2}, ra) = 0$
- ▶ Parameters: spacecraft and moon revolutions, the revolution of the maneuver, the departure/arrival configuration (In-Out)



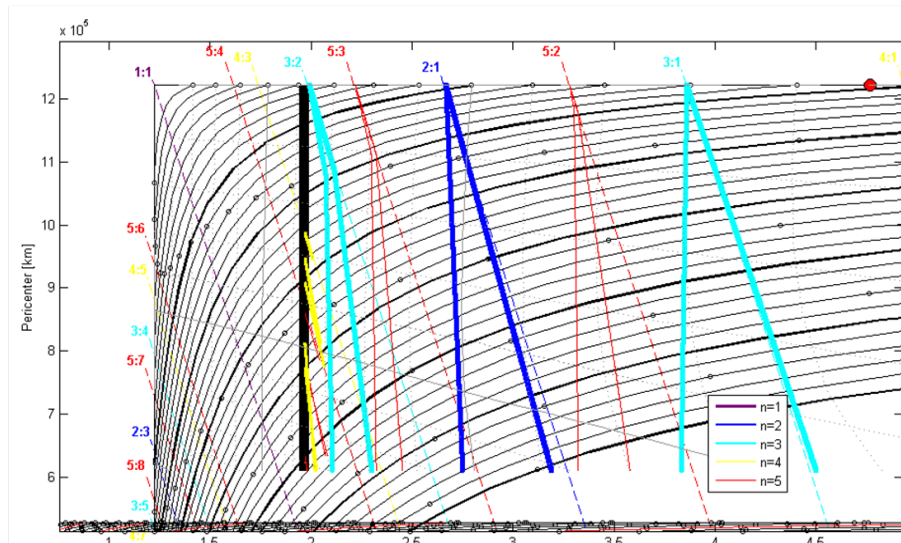
High Energy Transfers

- ▶ Starting with a given $v_{\infty 1}$, the solution space is a 1-dim manifold.
- ▶ *Actually, $2m + 2m$ 1-dim manifolds for each $n : m$ resonance*
- ▶ Solution manifold on the T-P graph; Linear approximation is accurate enough
- ▶ Method to compute linear solutions



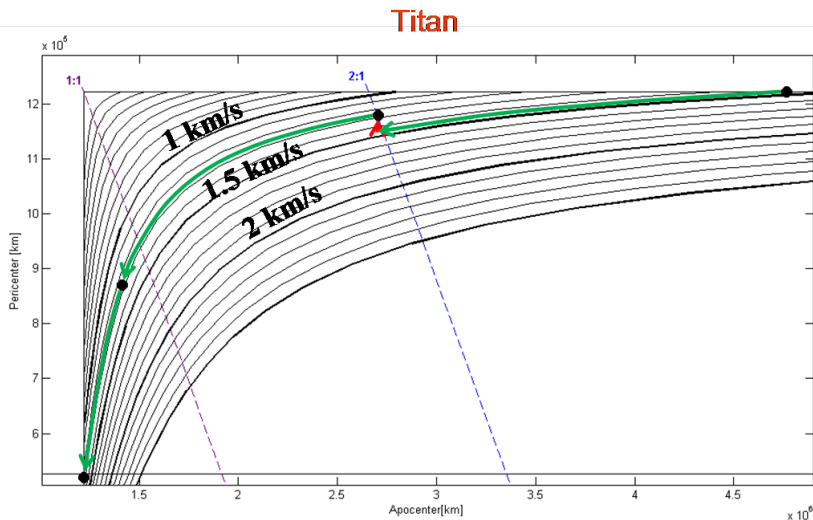
High Energy Transfers

Graphical method shows piecewise linear solutions which are the Pareto-optima of the linear approximations.



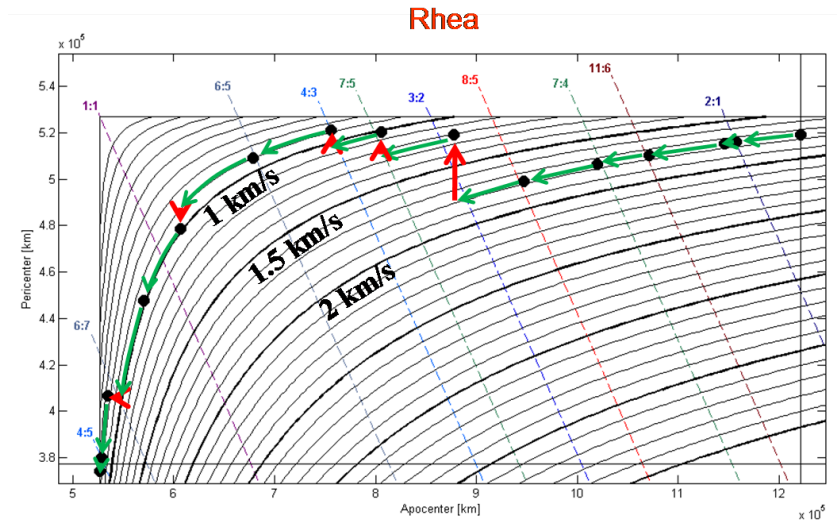
Titan-Enceladus

Staring from the first Titan's flyby to Enceladus Orbit Insertion



Titan-Enceladus

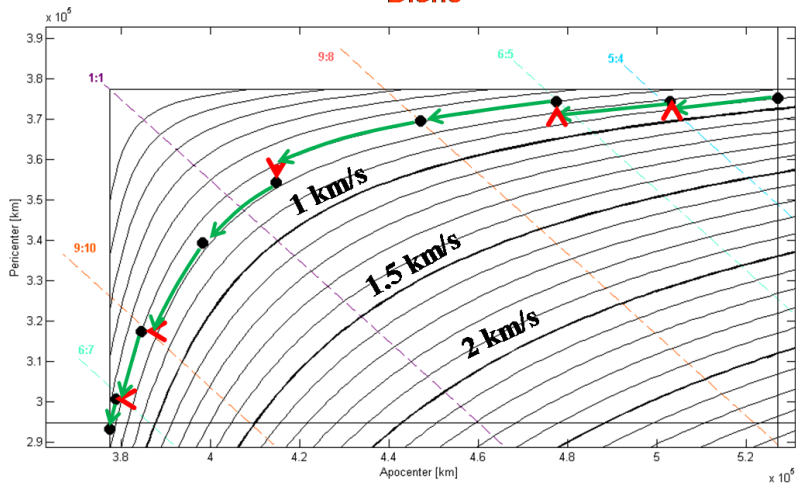
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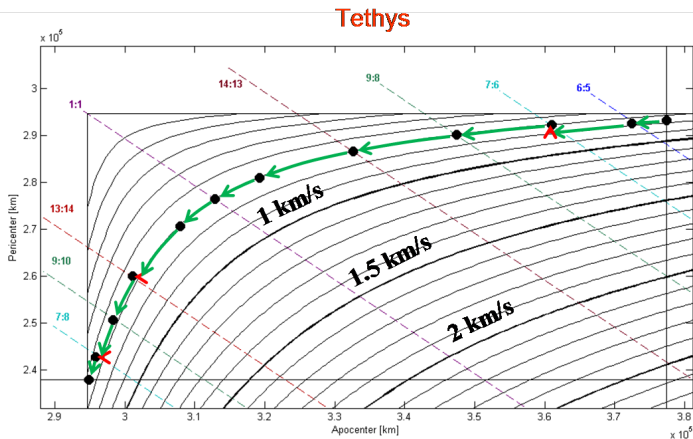
Staring from the first Titan's flyby to Enceladus Orbit Insertion

Dione



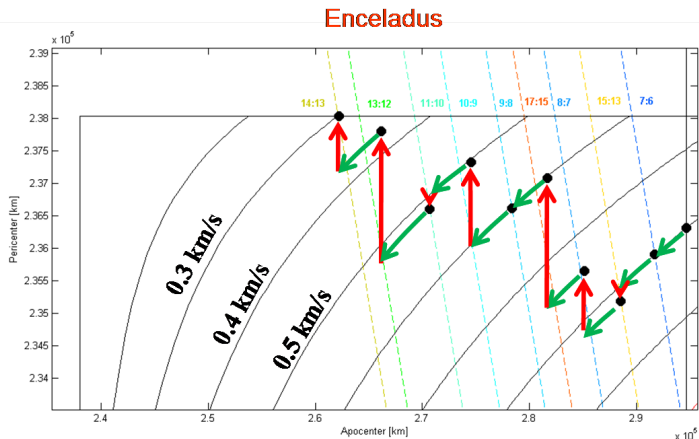
Titan-Enceladus

Starting from the first Titan's flyby to Enceladus Orbit Insertion



Titan-Enceladus

Starting from the first Titan's flyby to Enceladus Orbit Insertion



Titan-Enceladus

An Enceladus orbiter mission (alone or jointly with the Titan balloon mission) was considered **unfeasible** because the transfer from the first Titan's flyby would require **3.5 km/s or > 4 years**. We show that with **47 flybys and 0.7 km/s**, (including EOI), we arrive at Enceladus in **<2 years!**

Conclusions

- ▶ The T-P graph gives insight and a smooth transition between High-energy and a Low-Energy domain.
- ▶ Trajectory in the low energy domain have low ΔV , but high ToF because they start at high *altitudes*
- ▶ It is possible to transfer a spacecraft from a closed orbit near Europa and Ganymede at almost no ΔV , in eight months.

Consequences for the EJSM?

- ▶ Trajectories in the high energy domain have high ΔV , but lower ToF. They can be used efficiently in the phases that do not end with an orbit insertion. They *must* be used for small mass moons.
- ▶ Leveraging techniques allow to shorter the transfer time- an Enceladus orbiter is now a feasible option. **Consequences for TSSM?**